A scanning electron micrograph (SEM) of a microelectromechanical system (MEMS) device. The image shows a grid of circular structures, likely micromirrors, arranged in a regular pattern. A prominent, curved, metallic waveguide structure runs diagonally across the center of the image, connecting different parts of the device. The background is a light brown color, and the circular structures have a yellowish-gold center.

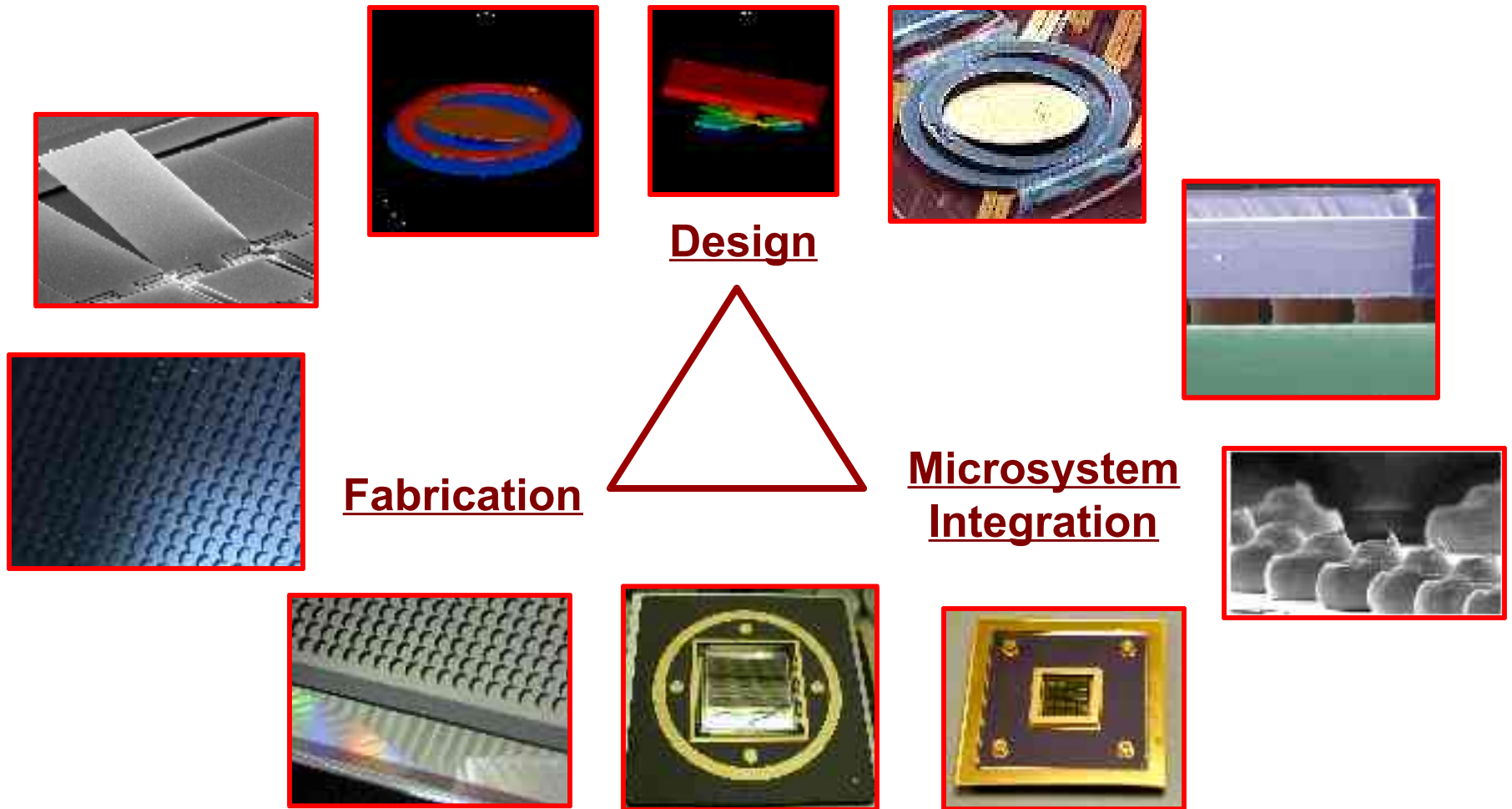
Optical MEMS: Actuating Light

V. A. Aksyuk

Microsystems Research

Bell Laboratories, Lucent Technologies

Optical MEMS at Lucent



Acknowledgements

MEMS devices: design, process, testing, reliability

S. Arney, H. Bair, C. Bolle, B. Barber, D. Carr, H. B. Chan, C. Chang, A. Gasparyan, R. George, L. Gomez, S. Goyal, D. Greywall, M. Haueis, T. Kroupenkine, V. Lifton, D. Lopez, M. Paczkowski, F. Pardo, A. Ramirez, R. Ruel, H. Shea, M. E. Simon, J. Vuillemin, J. Walker

Subsystem and System: optics, packaging, physical design, electronics, software, training & test

N. Basavanhally, R. Boie, C. Doerr, J. Ford, R. Frahm, D. Fuchs, J. Gates, R. Giles, J. Kim, P. Kolodner, J.S. Kraus, B. Kumar, C. P. Lichtenwalner, D.F. Lieuwen, Y. Low, D. Marom, D.T. Neilson, C. Nijander, C. J. Nuzman, R. Pafcheck, A. R. Papazian, D. Ramsey, R. Ryf, R. Scotti, L. Stulz, H. Tang, A. Weiss, J. Weld

NJ Nanotechnology Consortium (and formerly Si Fabrication Research Lab): MEMS processing, process development

G. R. Bogart, E. Ferry, F. P. Klemens, J. F. Miner, R. Cirelli, S. Rogers, J. E. Bower, R. C. Keller, W. Mansfield, C-S.Pai, W. Lai, K. Tefteau, H. T. Soh, J. A. Taylor, A. Kornblit, T.C. Lee and J. Q. Liu

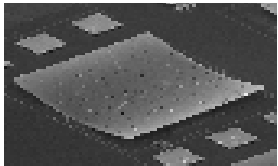
Leadership and support

S. Arney, J. Gates, R. Giles, D. Bishop

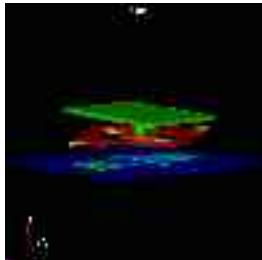


Optical MEMS at Lucent: Project Lineup

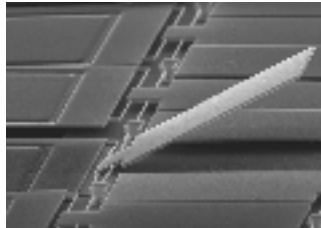
3 layer poly electrodes
bistable actuator
curvature mitigation
polarization controller
alternative flip-chip
control beyond snapdown
charging studies
dielectric leakage studies
MEMS reliability physics



1xN switch
waveguide 1x2 WSS
2D WSS
1D tilt OXC
party-favor mirrors



Double-hinge WSS
Fringe-field WSS
Torsional WSS
Si microlens arrays
Flag switch/VOA



Torsional blocker
LR 1296



LR 256
Agere 64 OXC



Research project

- idea demonstration
- approach verification
- numerical modeling
- process development
- basic reliability research

Device concept

- functionality demonstration
- design verification
- performance assessment
- reliability assessment

Device prototype

- subsystem demonstration
- detailed performance testing
- design optimization
- process optimization
- reliability testing

Models

- subsystem optimization
- design optimization
- manufacturability & yield
- subsystem reliability

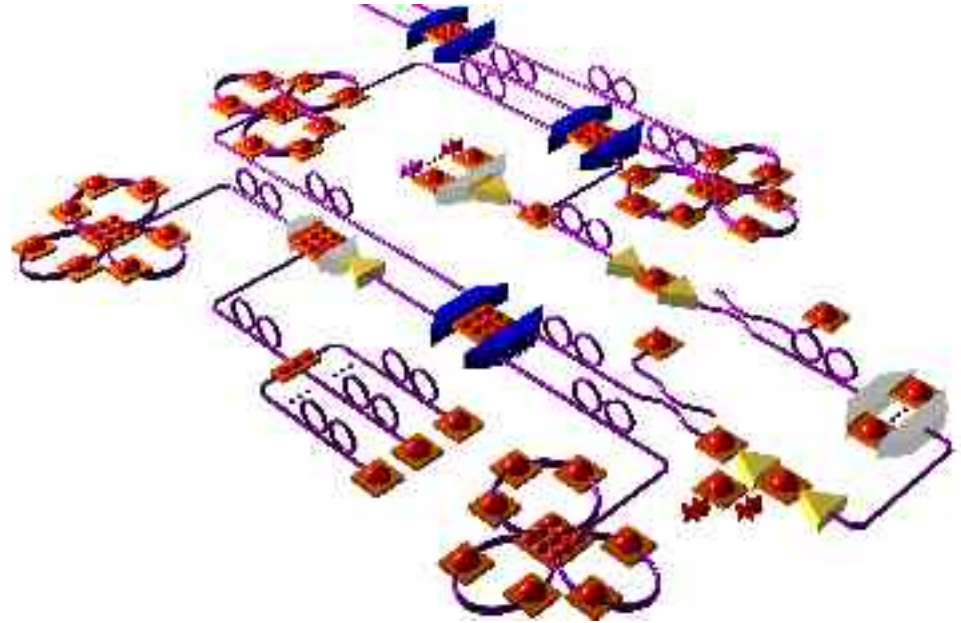
Product

- performance improvement
- yield optimization
- cost cutting
- troubleshooting
- reliability enhancement



Why Optical Micromachines ?

- Variable Attenuators
- Spectral Equalizers
- OLS Monitors
- Dispersion Compensators
- Data Modulators
- Protection Switches
- Add/Drop Multiplexers
- Crossconnects

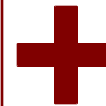


Excellent optical properties
of opto-mechanical
components:

- low optical loss
- high contrast
- wavelength independent
- polarization independent
- data format independent

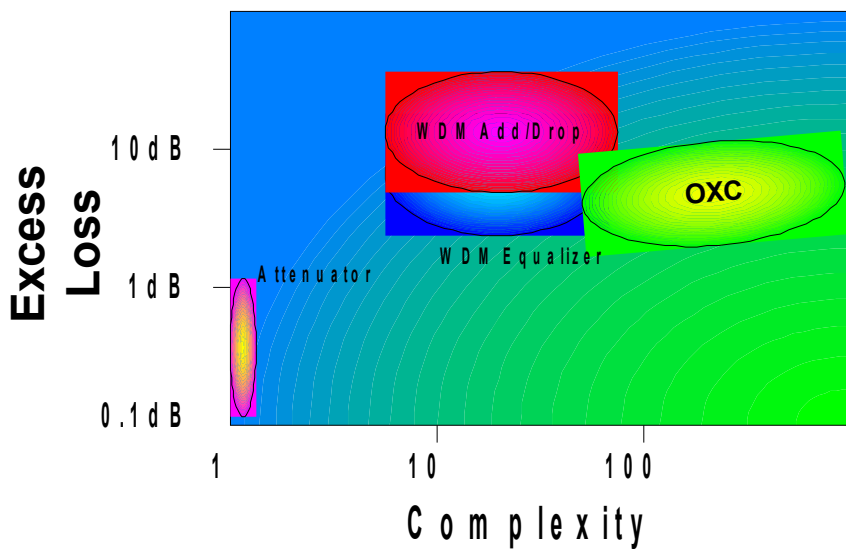
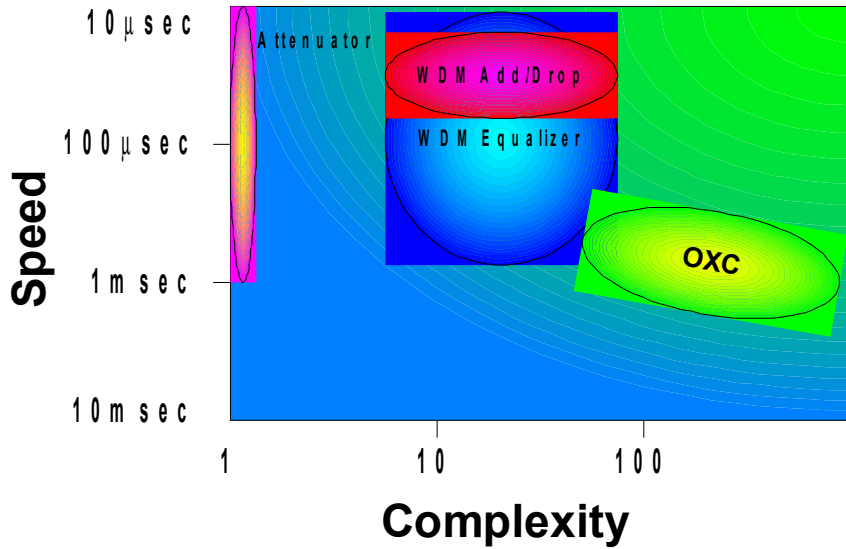
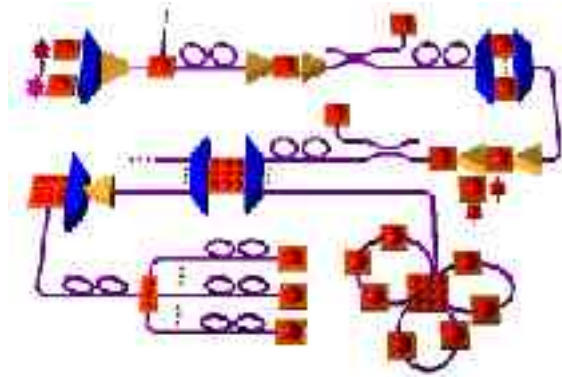


Thousands of
movable elements
(degrees of freedom)
on a single Si chip



Fast
Small
Inexpensive

Optical MEMS Application Space

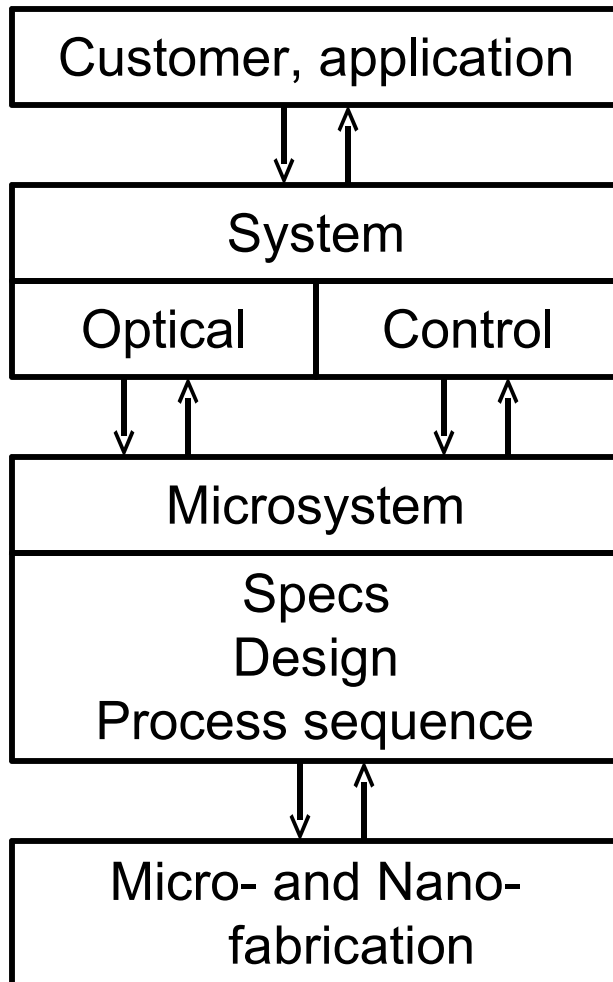


**High complexity devices -
optical subsystems with
new functions.**

**Low complexity devices -
optical components with
enhanced performance
and features.**

Complexity is a measure of either function or number.

Microsystems Enable Integrated Solutions



Expertise required:

Application knowledge

System architecture

Optics

Electronics & Control

Packaging

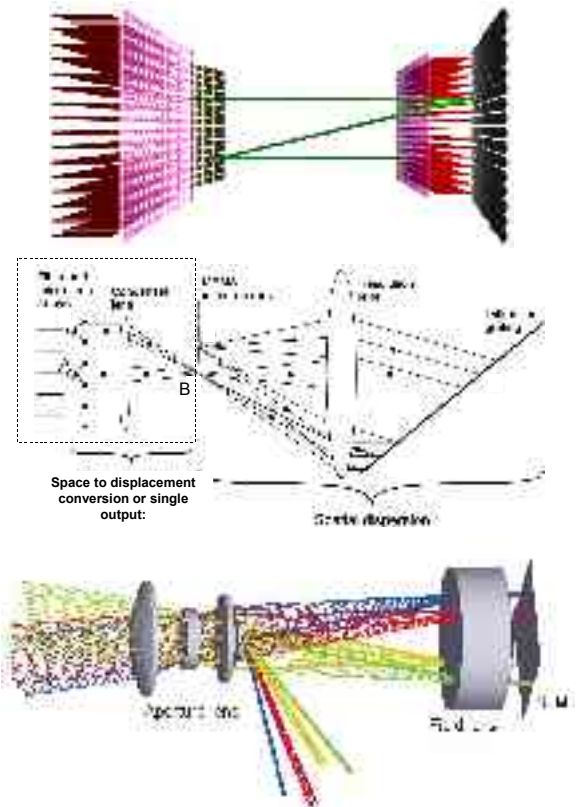
Microsystems:

- Design
- Micro- Nano- fabrication
- Test and Characterization

Application Space

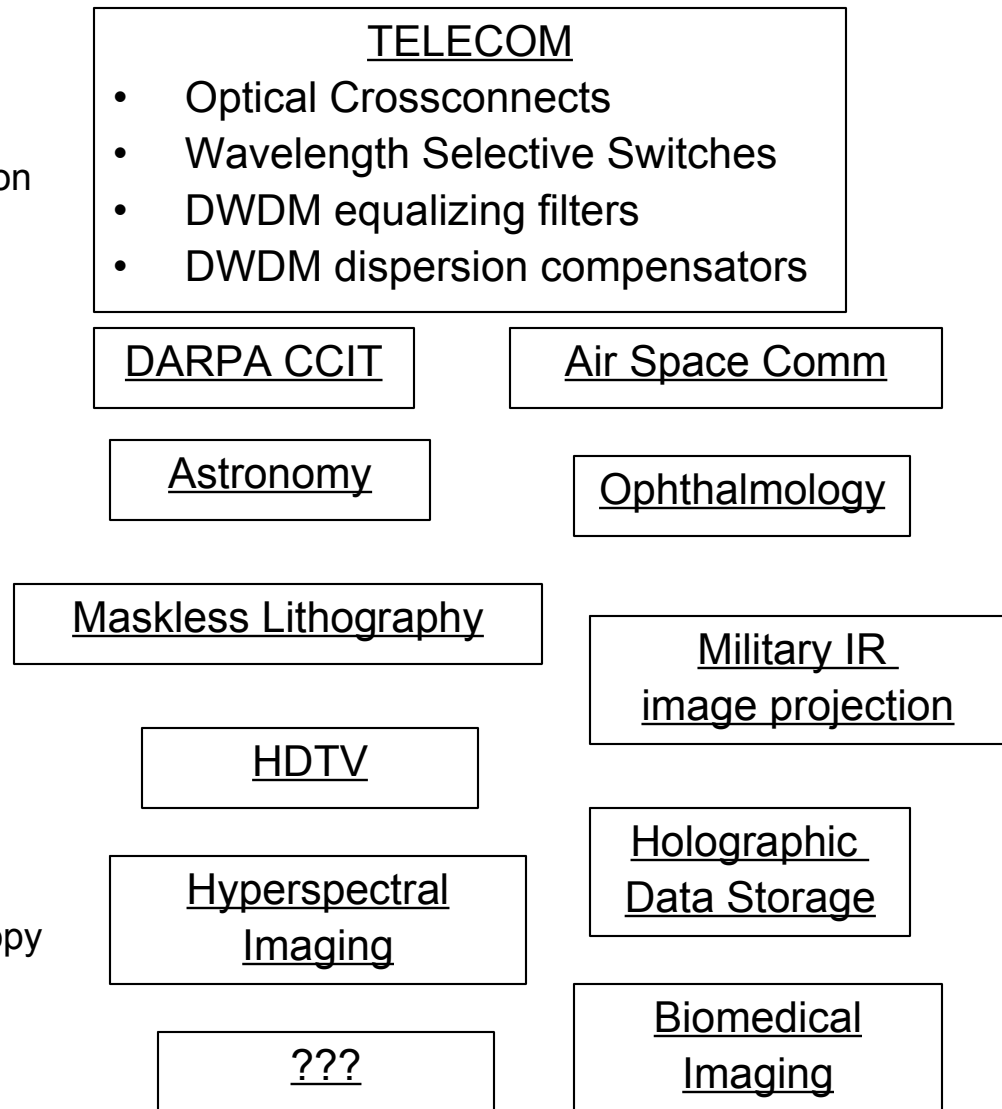
The GOAL is to realize Microsystems unique benefit – to combine a huge number of degrees of freedom in a single device, enabling unprecedented degree of control over optical signal(s):

- 100's of channels
- 100's of wavelengths
- Millions of pixels
- Extremely complex wavefront manipulation
 - Point
 - Focus - multiple sources or targets
 - Track
 - Correct aberrations and distortions
 - Process information optically



Addressable Application Space Diversity

- Optical switching
 - Distinct optical channels
 - Distinct wavelength
 - Dynamic DWDM filtering and dispersion compensation
- Free space optical
 - Communication
 - Imaging
 - Targeting
- Adaptive optics
 - Distortion correction for imaging
 - Metrology
- Projection
 - (Deep) UV
 - Visible
 - IR
- Digital Holography
 - Optical data storage
 - Spectroscopy and imaging spectroscopy
 - Optical information processing
 - Optical tweezers and manipulation
 - Other imaging and metrology



Optical Microsystems Technologies: Examples

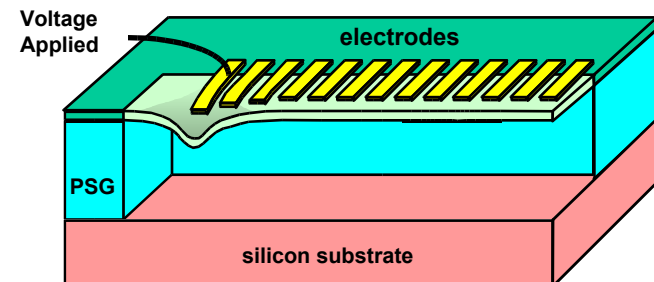
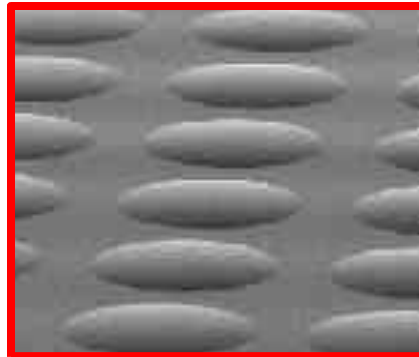
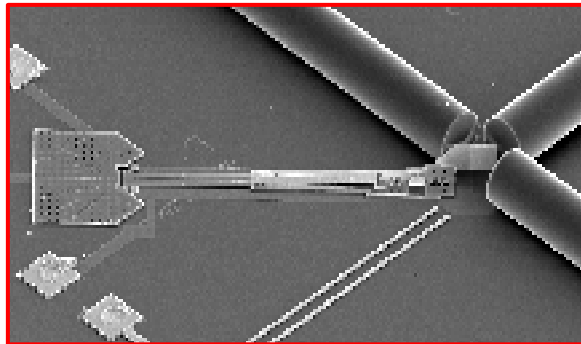
Large arrays of movable mirrors - **reflective**

Tunable reflectivity **interferometric** devices

Si microlens arrays - **refractive**

Variety of other devices (e.g. **diffractive**)

See e.g. J.Ford, Hilton Head 2004

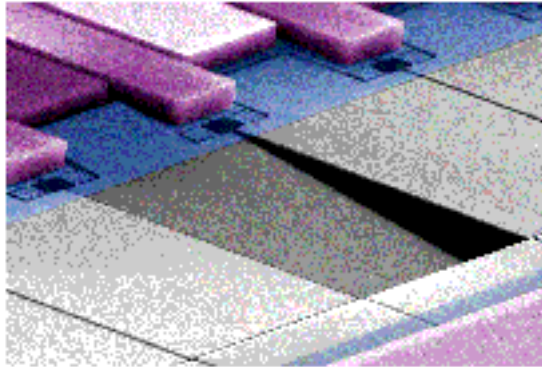


Application example: Telecom

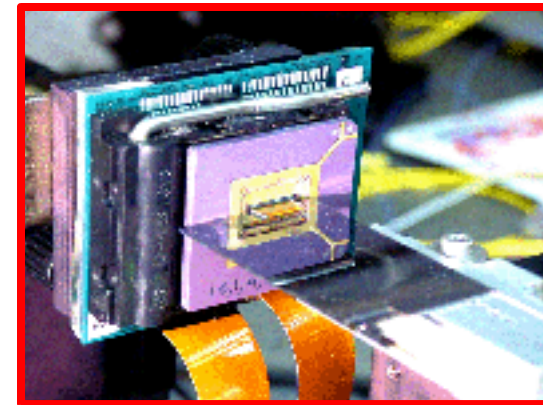
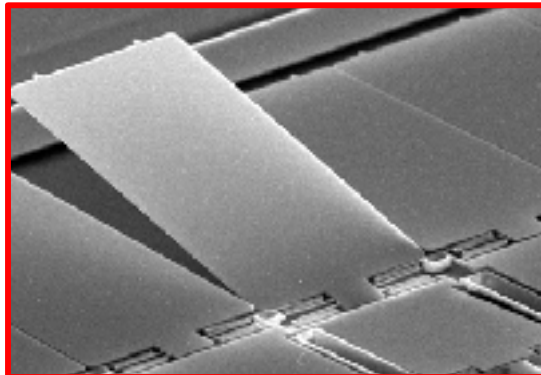
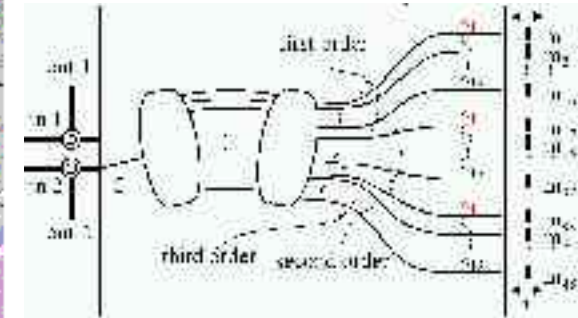
Lambda router



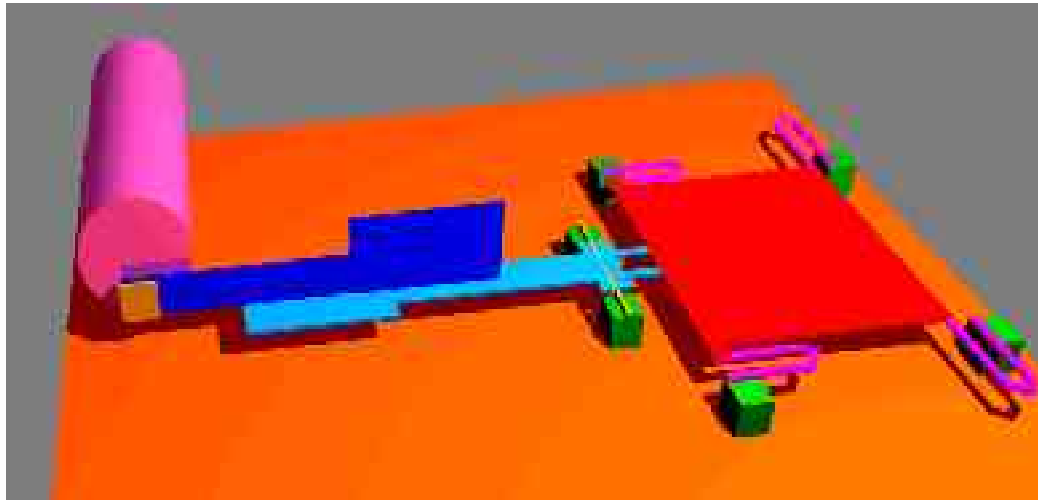
Wavelength selective switch



MEMS and Waveguides

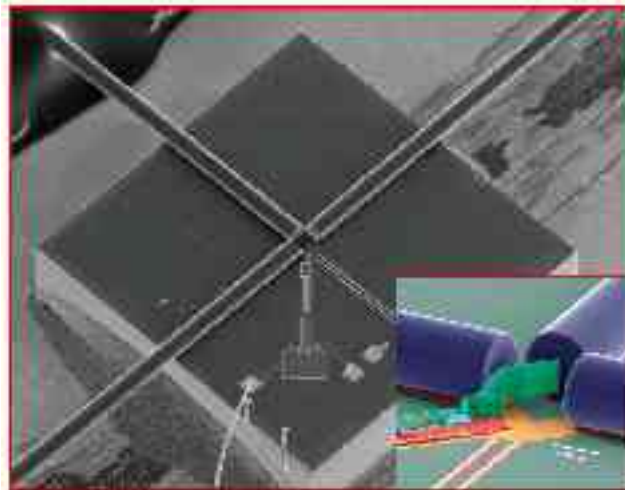
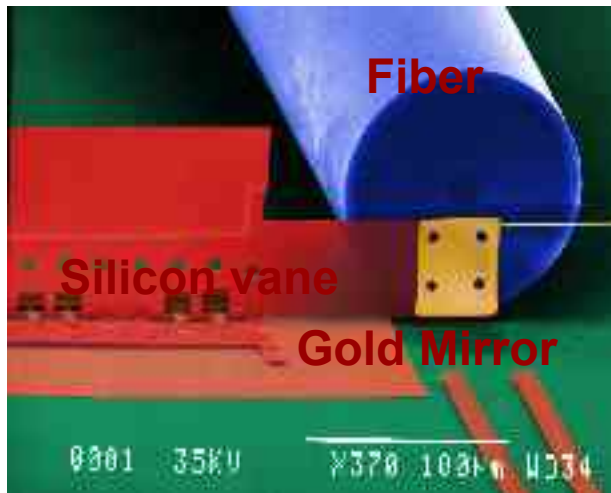


Electrostatically Actuated MEMS Switch



Gold Reflector enters Optical Path

Spring-suspended capacitor plate

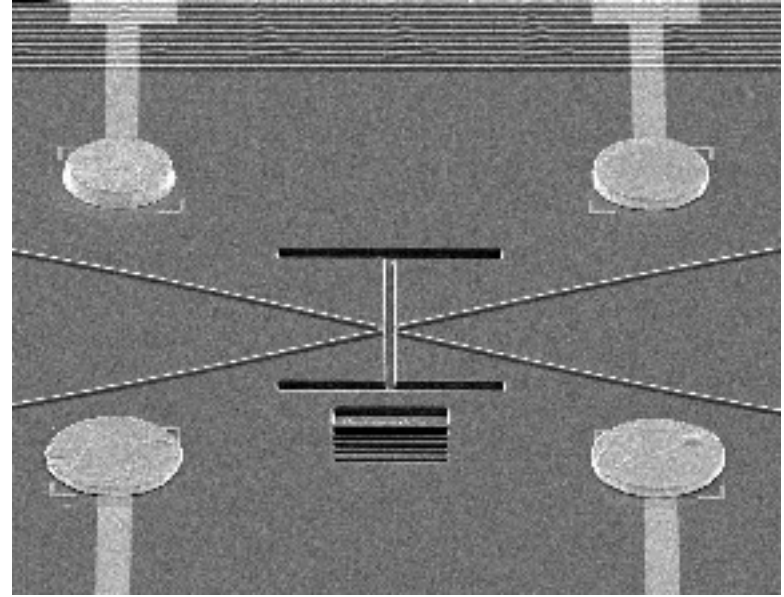
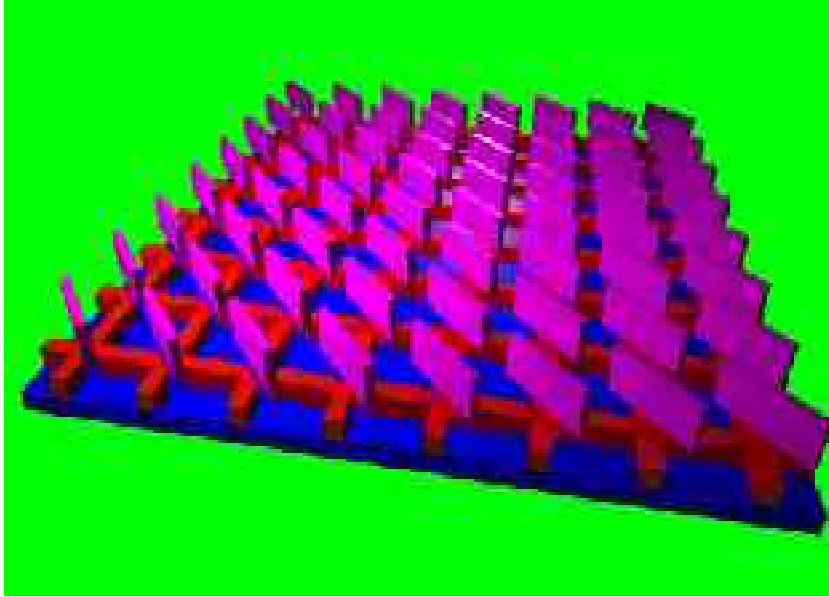


- <math><70\ \mu\text{sec}</math> response
- 1.24-20V actuation (design dependent)
- supports attenuator function

- 1x2 optical switch
- <math><1.5\text{dB}</math> loss with passive alignment
- <math><1.0\text{dB}</math> loss with active alignment



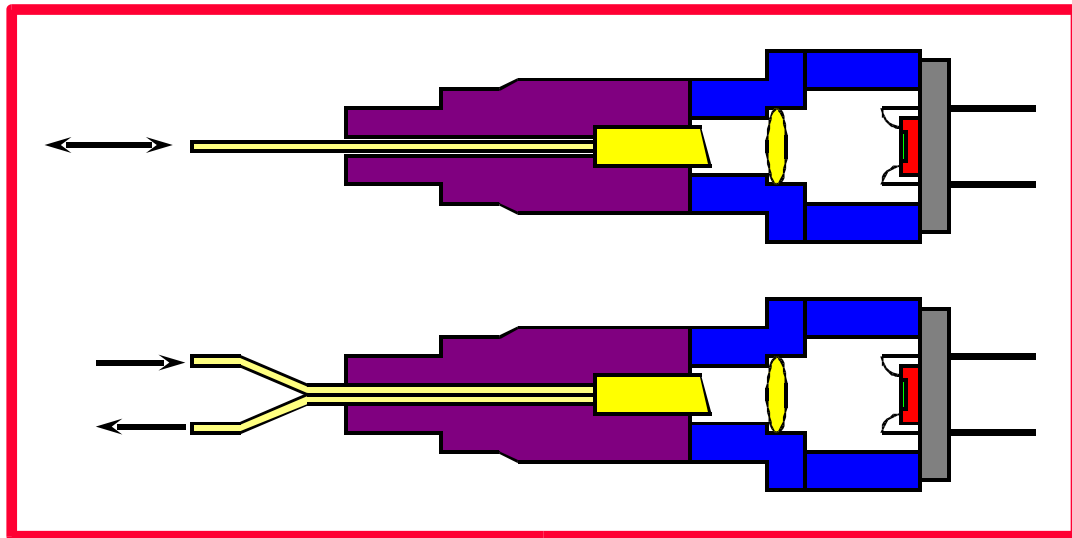
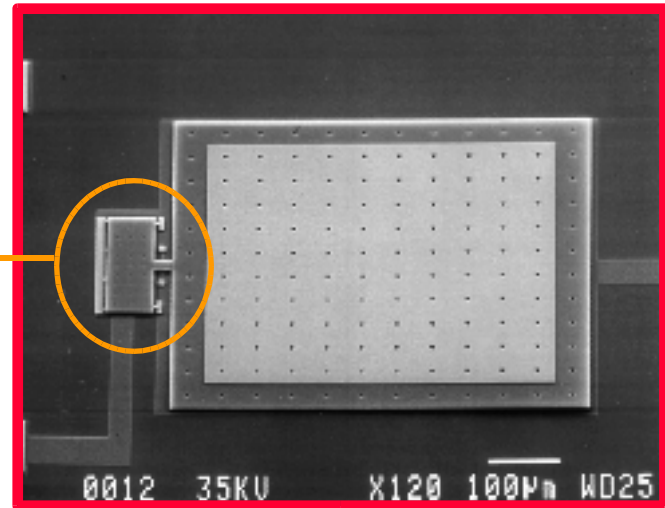
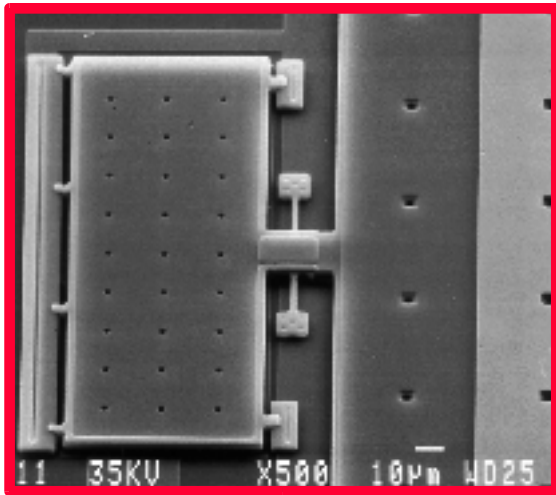
Flag switch combined with waveguide technology



Not practical for large single-stage optical crossconnect, but small switches and other new subsystems are possible.



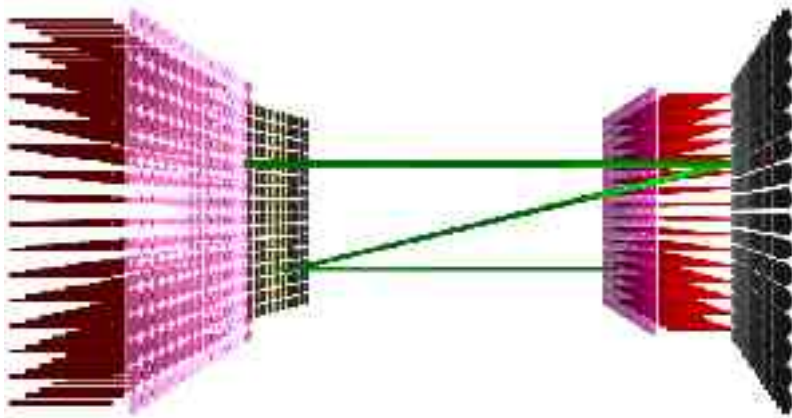
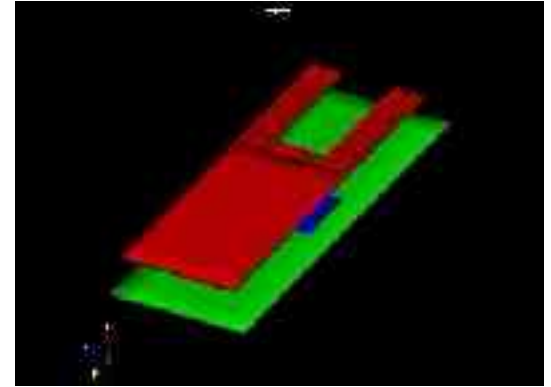
Tilt-Mirror Variable Attenuator



- operating power ~1nW
- insertion loss ~0.5dB
- PDL < 0.1dB
- speed < 1msec
- cost ~low
- size 1x0.5x0.5 cm³
- spectral flatness < 0.2dB
- dynamic range ~20dB

Optical MEMS for Telecom:

- Quality optical elements
- Precision actuators
- Speed
- High reliability



- Large number of elements
- High integration density

Key design features:

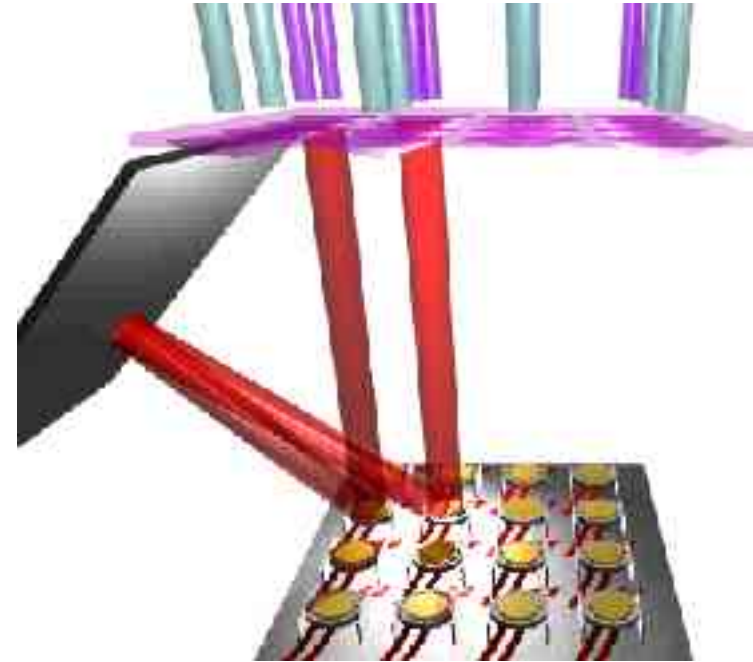
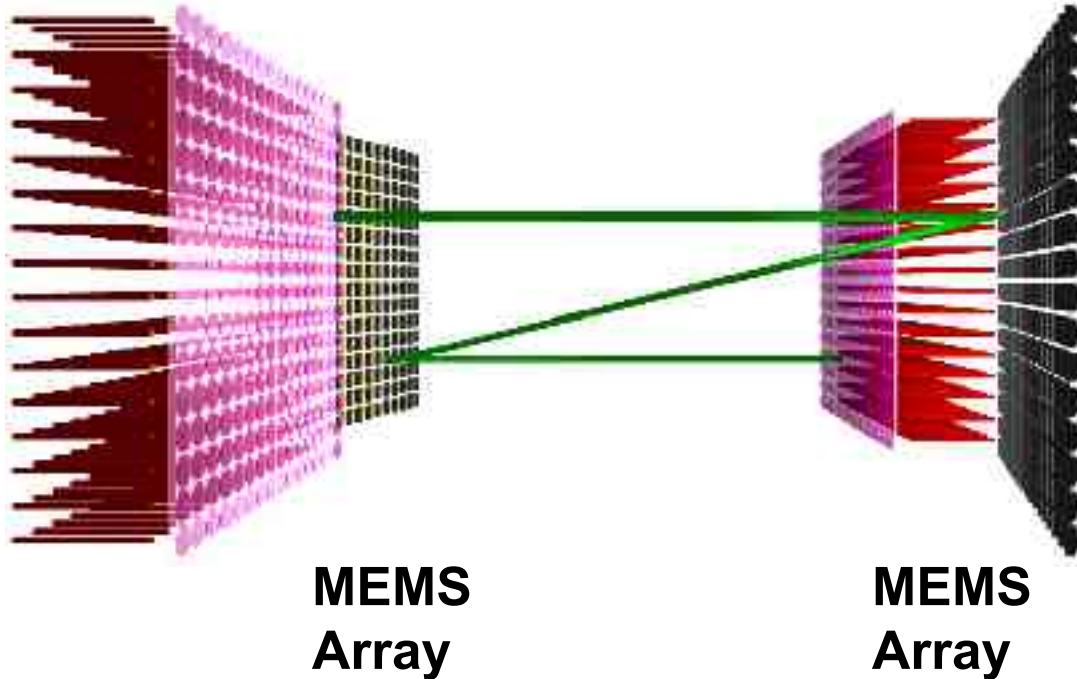
compliant mechanisms, electrostatics, stress engineering

Nonlinear Effects - Numerical Modeling

MEMS OXC -- 3D Architecture

Output Ports

Input Ports



512 MEMS mirrors in an 256x256 single-mode fiber optical crossconnect.

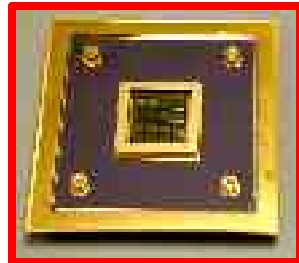
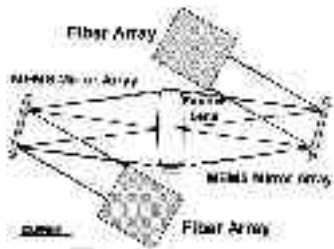
**16 mirrors in an 8x8 OXC
Folded optical design**

1.55 or 1.3 um single mode
Less than 5 msec switching
Low insertion loss

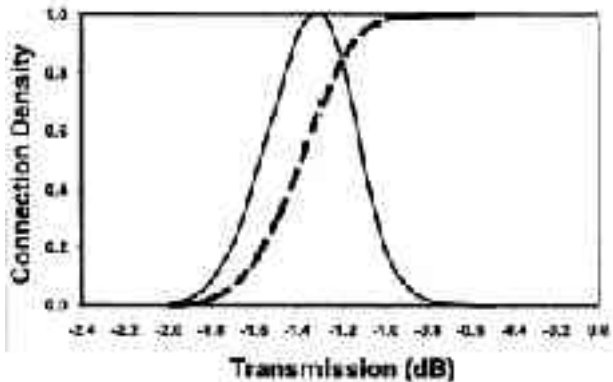
2N scaling
Non-blocking architecture
Single stage



MEMS OXCs – Big and Bigger

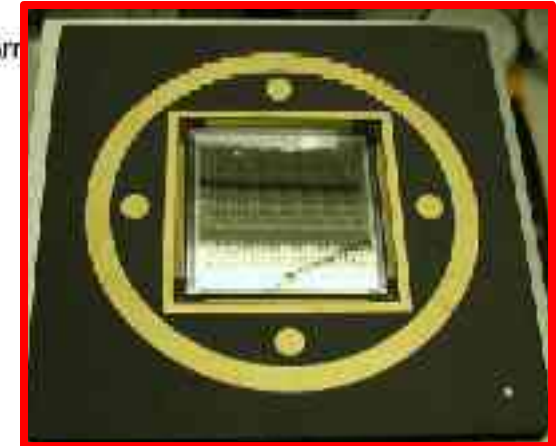
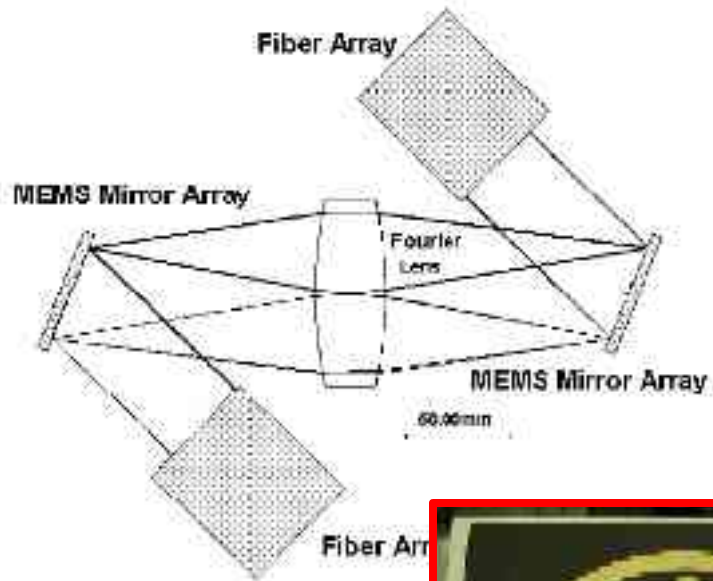


256 mirrors



238x238 ports

- 56,644 connections
- 1.33 dB mean loss
- 2.0 dB maximum loss

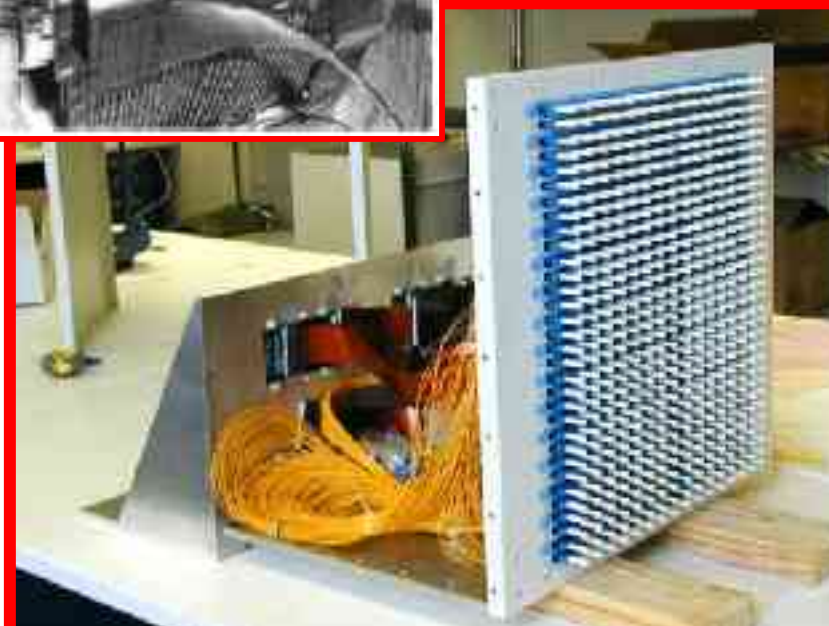
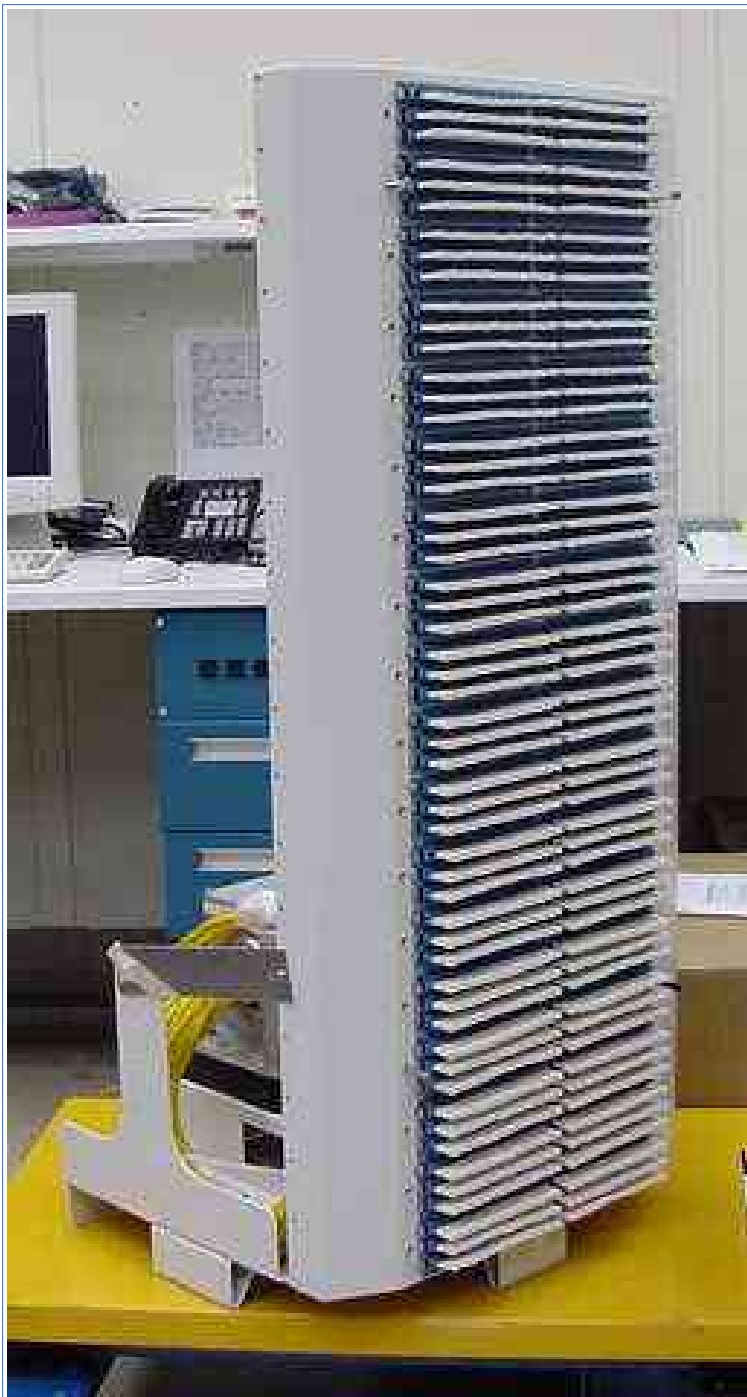


1100x1100 ports

- 1,210,000 connections
- 2.1 dB mean loss
- 4.0 dB maximum loss

1296 mirrors

Optical Switch Fabrics



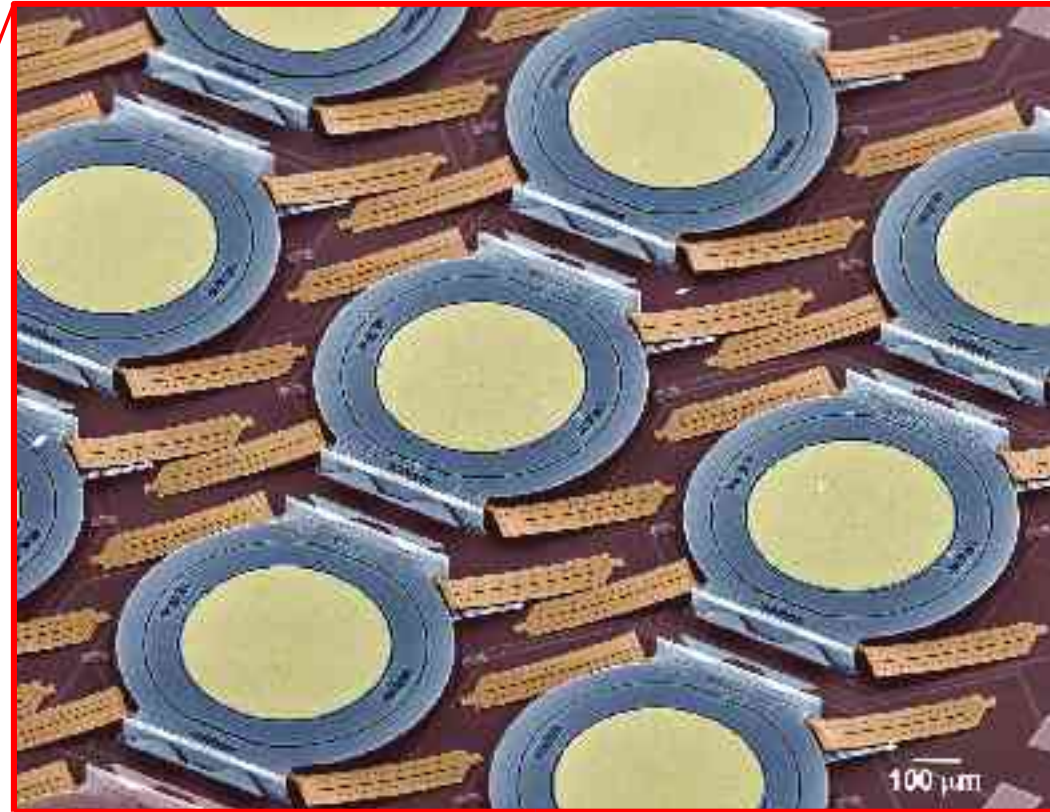
MEMS Device Requirements

Device:

- 2-axis, large angular range
- continuous, controlled tilt
- high quality, large reflectors
- wavelength independent

Technology:

- scalable
- well-established
- manufacturable

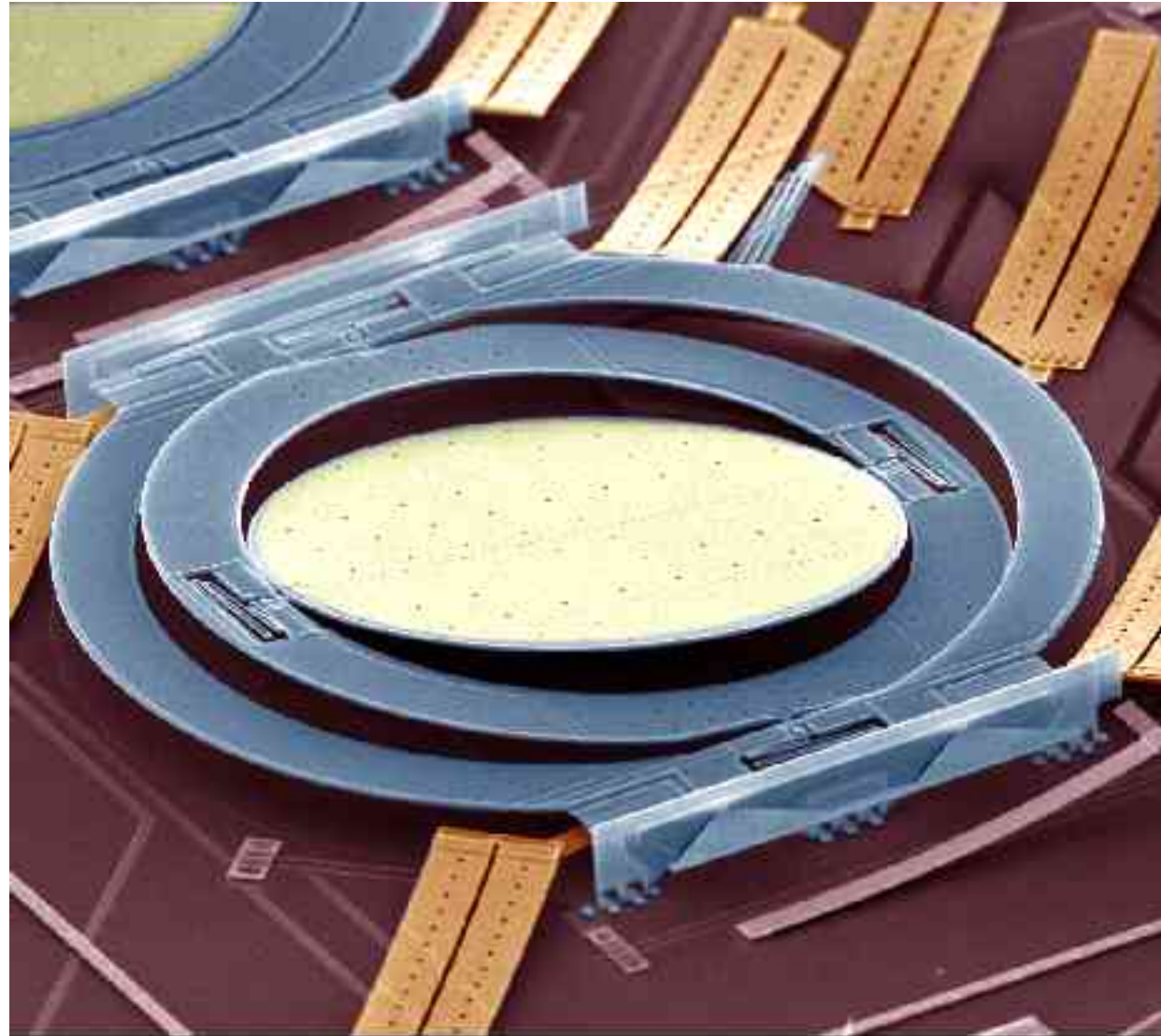


2-axis Beam-Steering Surface-Micromachined Mirror

Lucent Technologies
Bell Labs Innovations

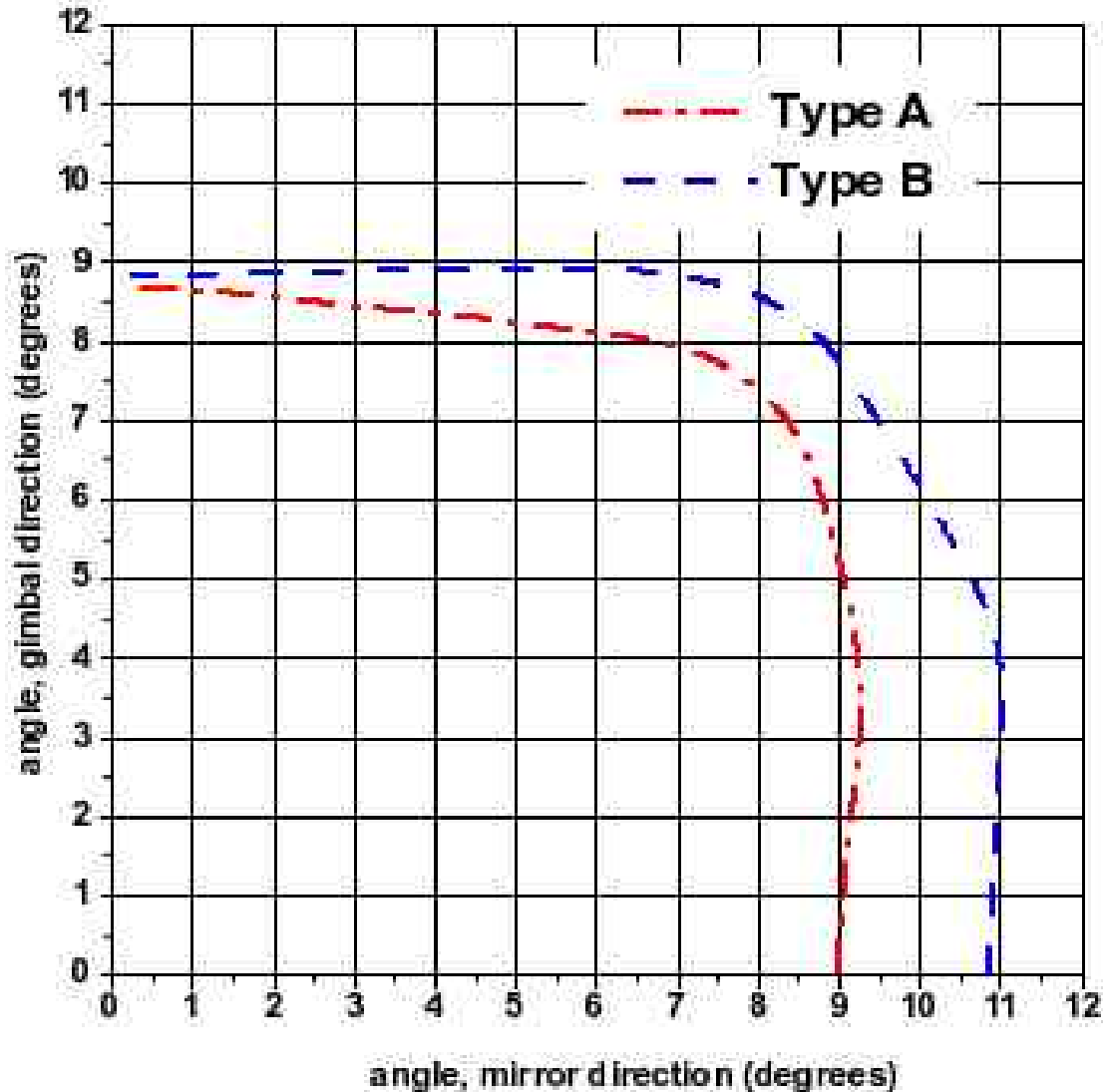


- raised frame for $\pm 9^\circ$ angles with 500um reflector
- self-assembly mechanism to lift and lock the frame
- gimbal mount with four serpentine springs
- electrostatic actuation with electrodes under device
- < 170V drive voltage to capacitive load
- < 5msec switching time
- gold reflector

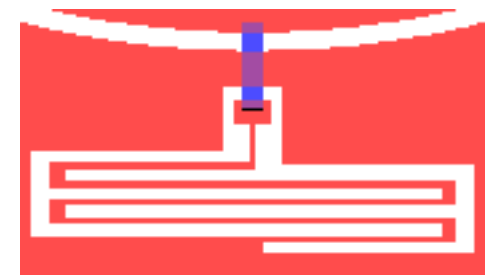


Mirror Deflection Range

500um surface-micromachined mirror



Type A
Pure flexure, simple



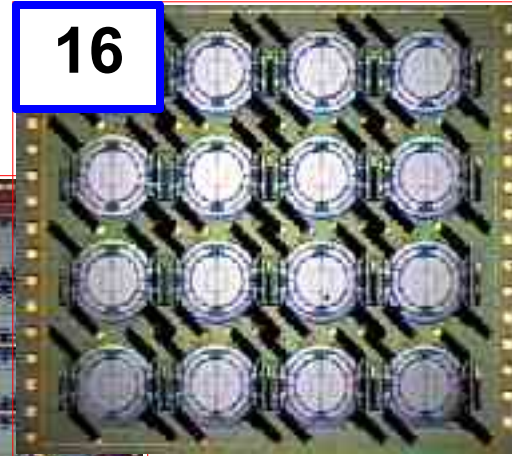
Type B
*Microbearing,
greater range*



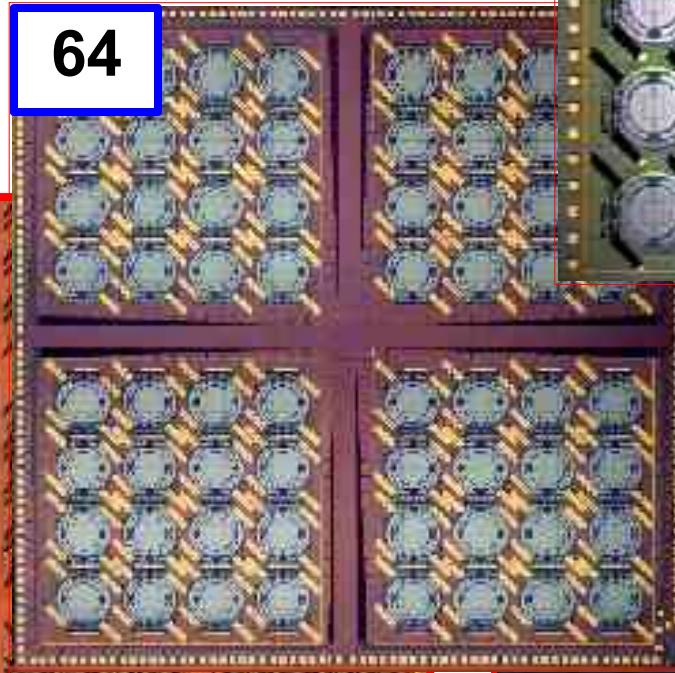
Micromirror Arrays



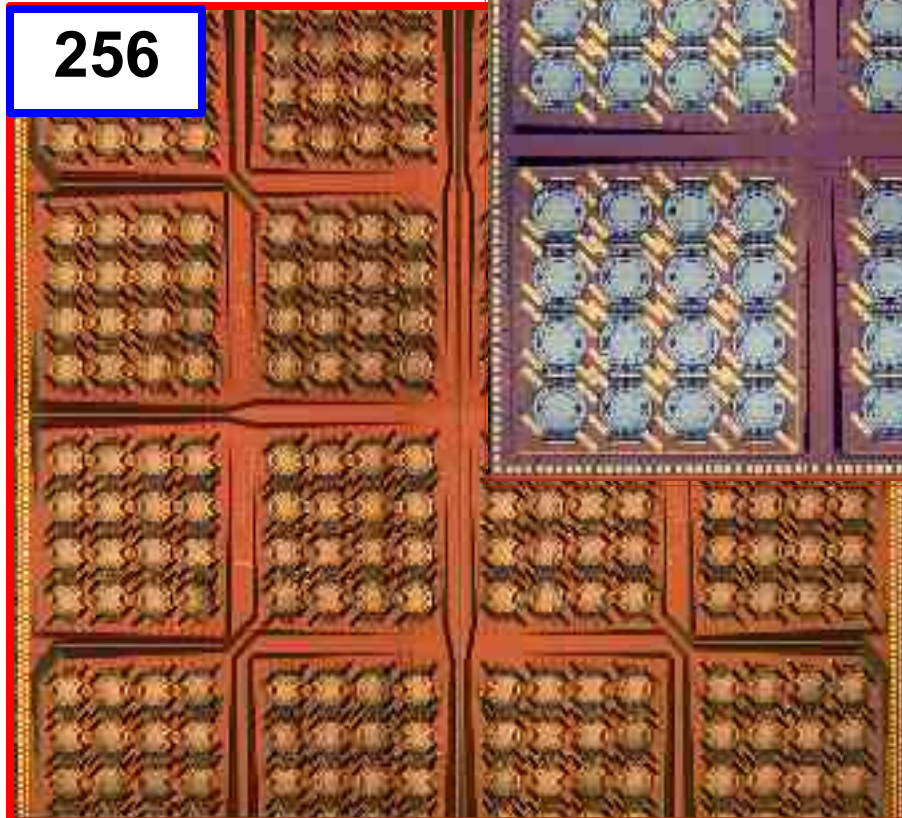
16



64



256

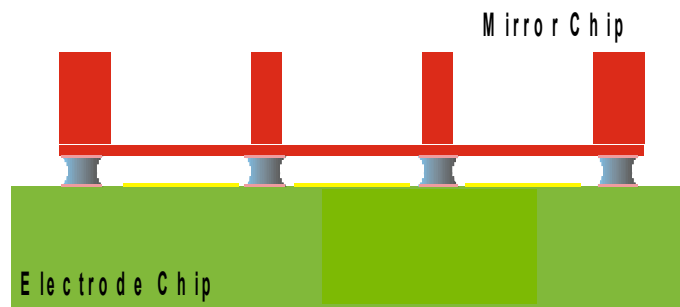
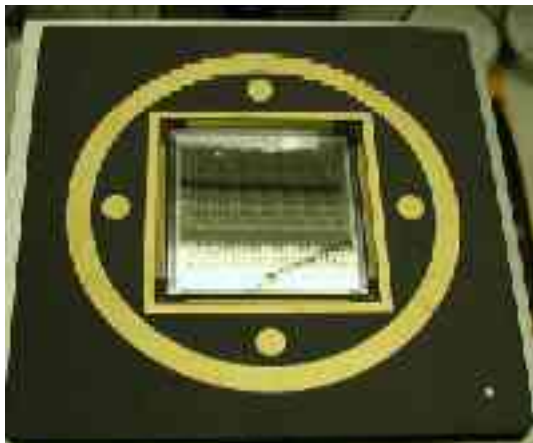
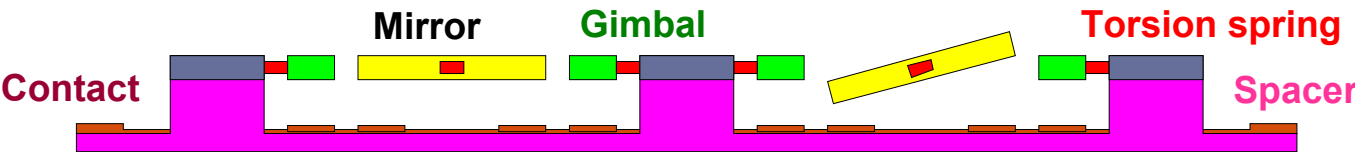
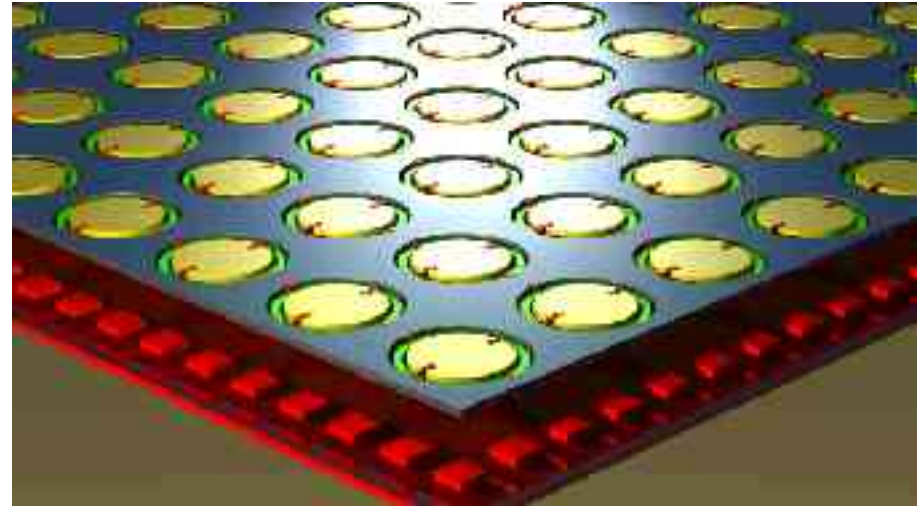


1296

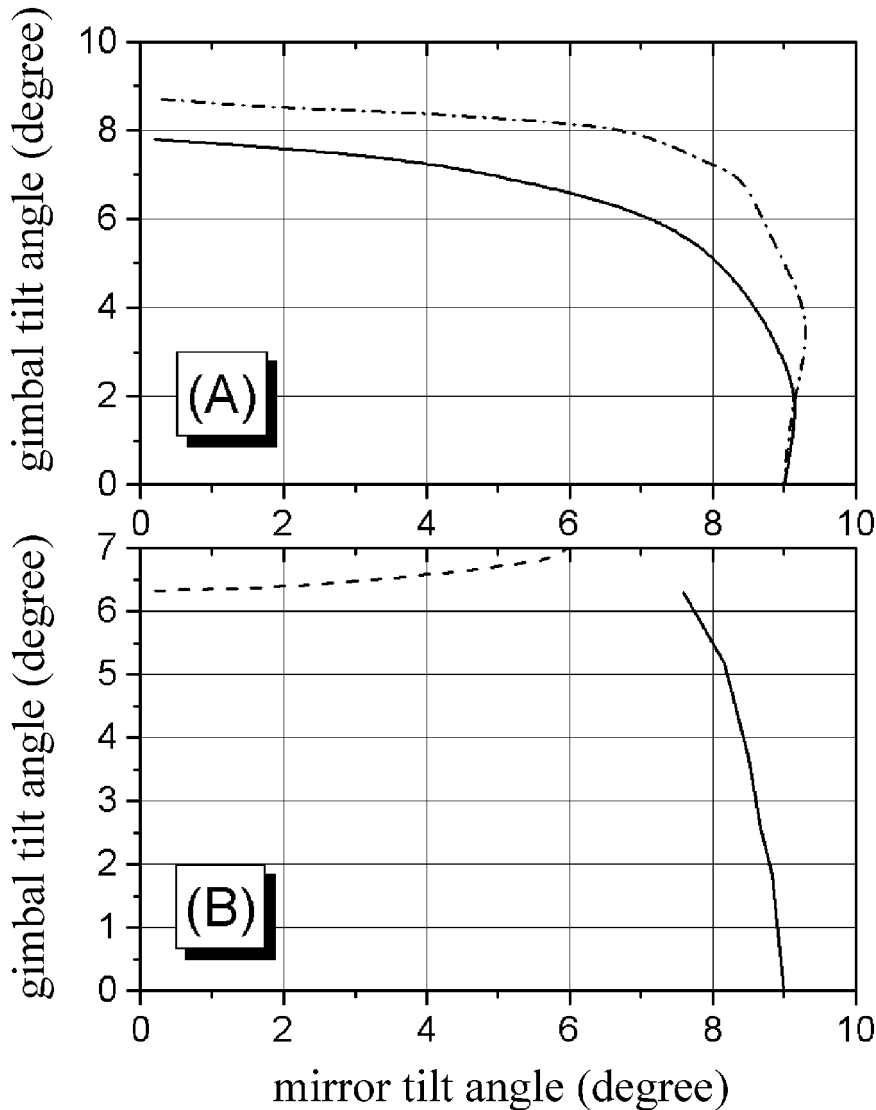


Single-Crystal Silicon Micromirrors

1296 mirror array (36x36)



Mirror Deflection Range Comparison



(A) Surface-micromachined mirrors (1 mm pitch):

- **Solid curve – 500um reflector**
- **Dashed curve – 600um reflector**

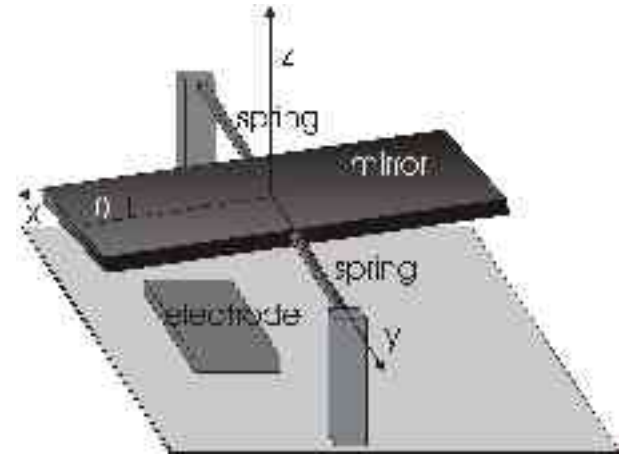
(B) SOI mirror (875um reflector, 1.25 mm pitch):

- **Solid curve – stability range**
- **Dashed curve – 200V range**

Beam-Steering Micromirror Design

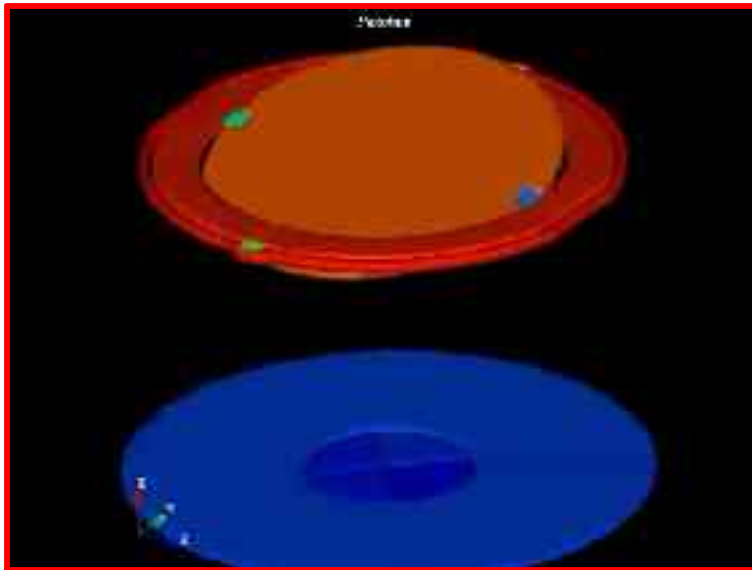
Design parameters:

- Electrode size and shape
- Gap size
- Spring and gimbal geometry
- Mirror thickness



Device characteristics:

- Angular range
- Mirror size
- Mirror shape - flatness
- Integration density - fill factor - **no crosstalk**
- **Spring stiffness** - speed - vibration sensitivity
- **Drive voltage, angle vs. V curve** - control
- Stability and repeatability
- Reliability



Electrostatics:

$$E = \frac{1}{2} V_i V_j C_{ij}; \quad \text{Torque: } T_l = \frac{\partial E}{\partial l}$$

Mechanics:

$$T_l = K_{lm} \delta_{lm}$$

Equilibrium:

$$K_{lm} = \frac{1}{2} V_i V_j \frac{\partial C_{ij}}{\partial l}$$

Stiffness matrix linear, diagonal;
same springs for x and y:

$$K_{lm} = 0$$

$$T_l = \frac{1}{2} V_i V_j \frac{\partial C_{ij}}{\partial l}$$

Dynamics:

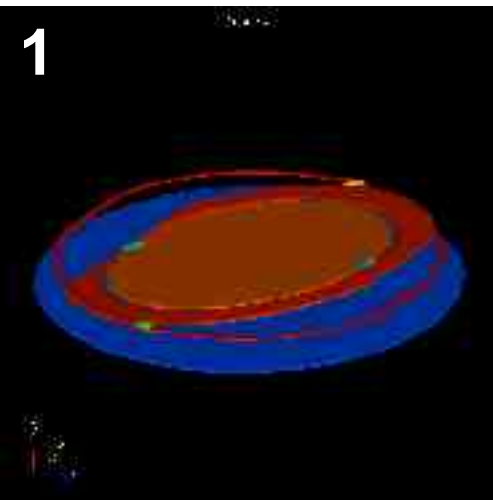
$$I_{lm} \ddot{\theta}_l = \frac{1}{2} V_i V_j \frac{\partial C_{ij}}{\partial l} - T_l$$

x, y collinear with main
axes of inertial tensor I:

$$I_{lm} = I_l \delta_{lm}$$

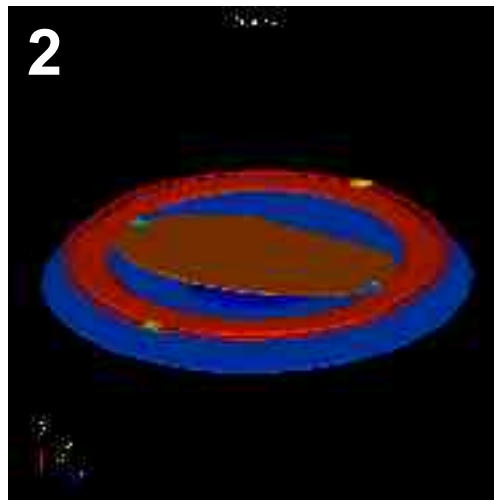
$$\text{for } l=1,2 \text{ (no summation in } l\text{): } I_l \ddot{\theta}_l = \frac{1}{2} V_i V_j \frac{\partial C_{ij}}{\partial l} - T_l$$

Resonance Modes



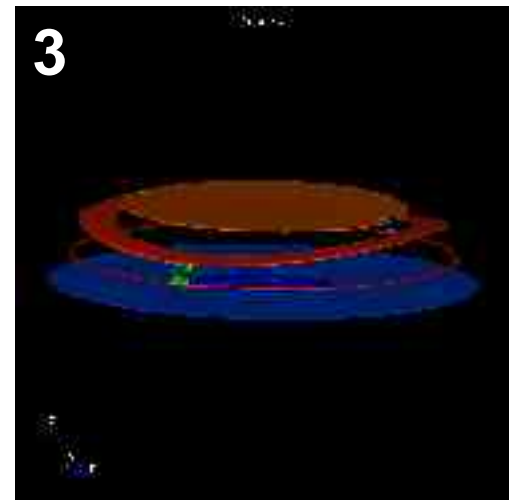
258 Hz

2153 Hz



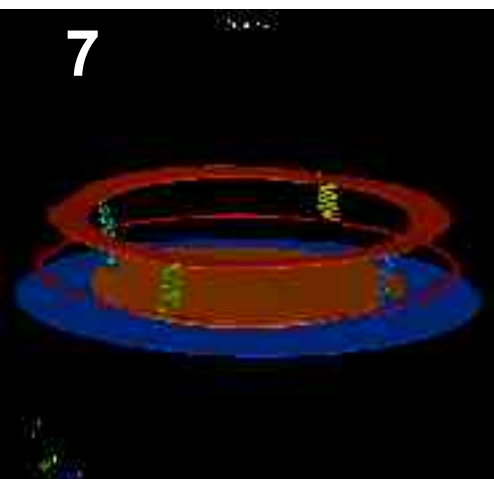
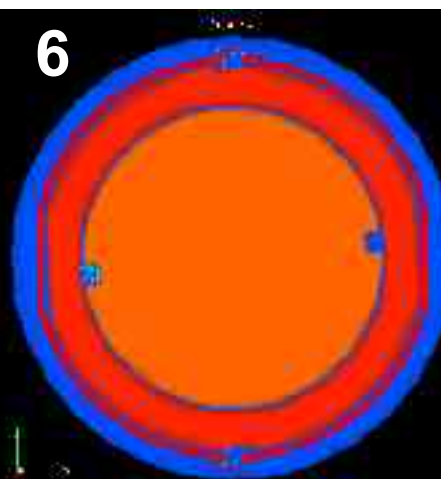
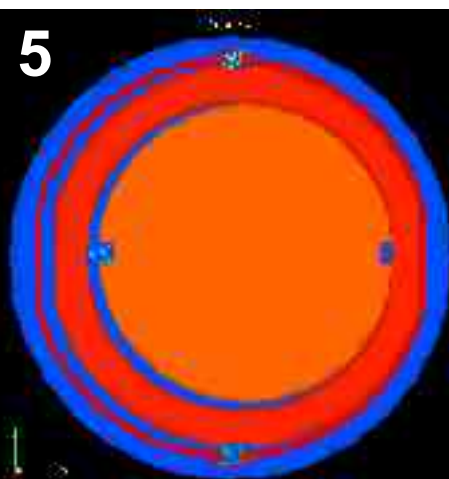
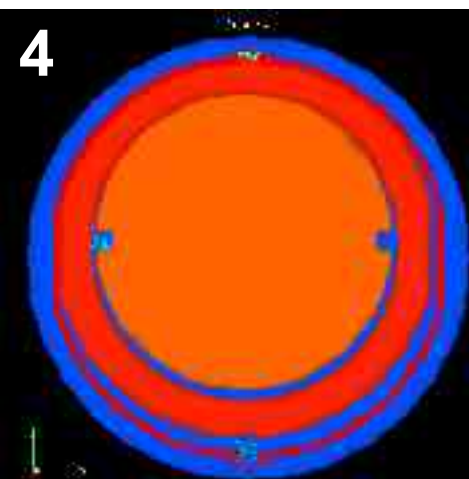
430 Hz

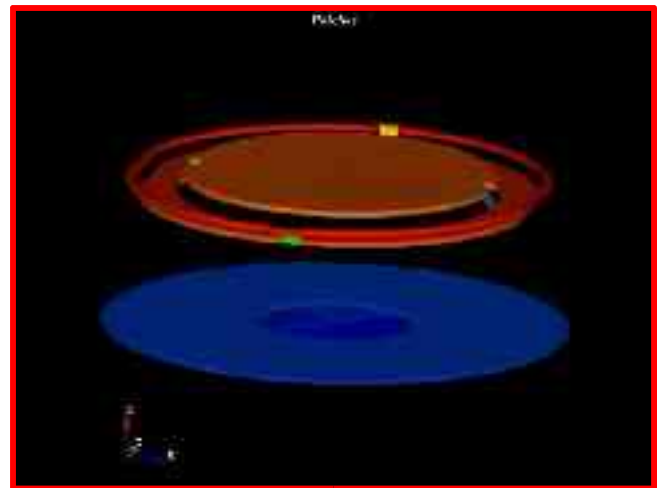
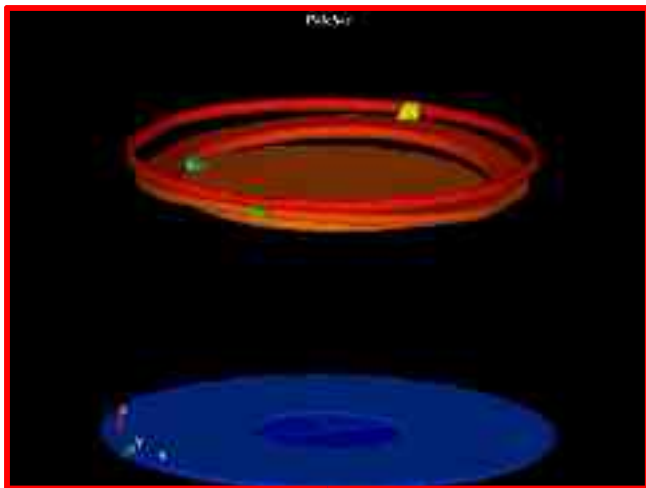
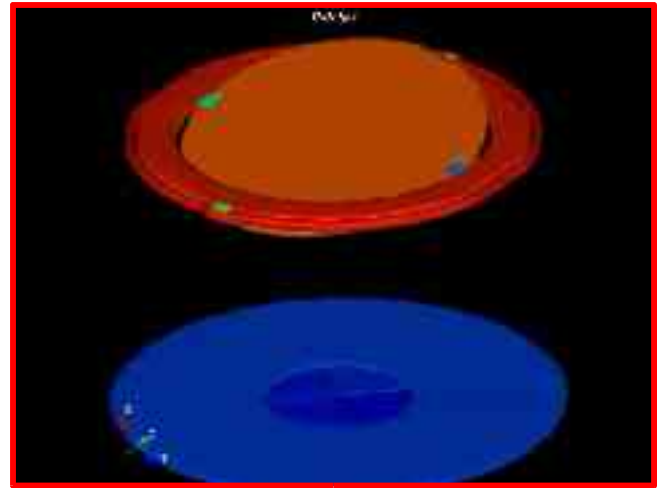
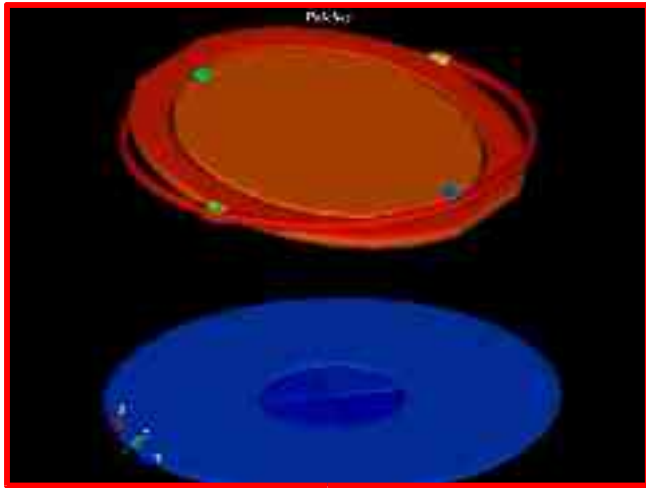
2345 Hz



1786 Hz

6869 Hz





Mode frequencies; crystalline direction dependence

Mode #	1	2	3	4	5	6	7
100 (45 degrees)	258	430	1786	2153	2345	3586	6869
110 (90 degrees)	286	477	1881	2409	2632	4048	7239
100 Experiment	260	430	1700				6900

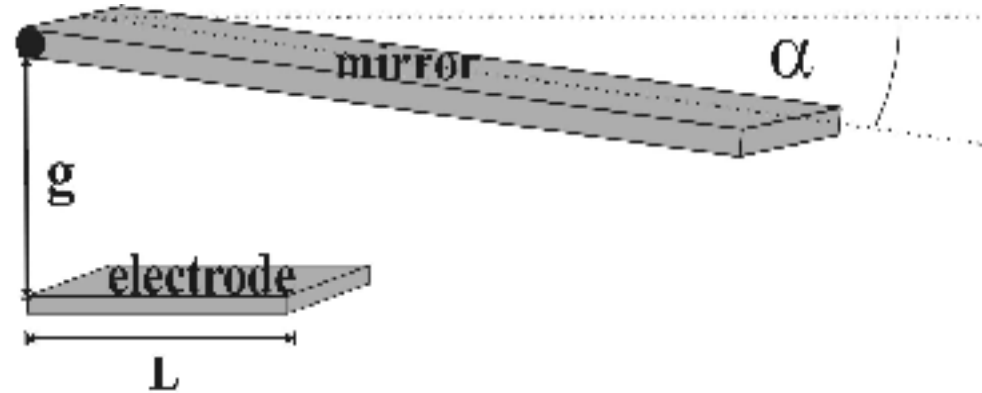
Approximation - beam X-section rectangular, $w = (a+b)/2 = 1.6\mu\text{m}$
instead of real-life trapezoidal $a = \mathbf{1.4\mu\text{m}}$, $b = 1.8\mu\text{m}$.

Si elasticity tensor components:

$$\lambda_{xxxx} = 165.5 \text{ GPa}, \lambda_{xyxy} = 64.18 \text{ GPa}, \lambda_{xyxy} = 79 \text{ GPa}$$

Analytical

Disregard Fringe Effects



$$T_{\text{electrostatic}} = \frac{\epsilon}{2} V^2 \int_0^L \frac{xW(x) dx}{\left(\frac{g}{\sin \alpha} - x \right)^2}$$

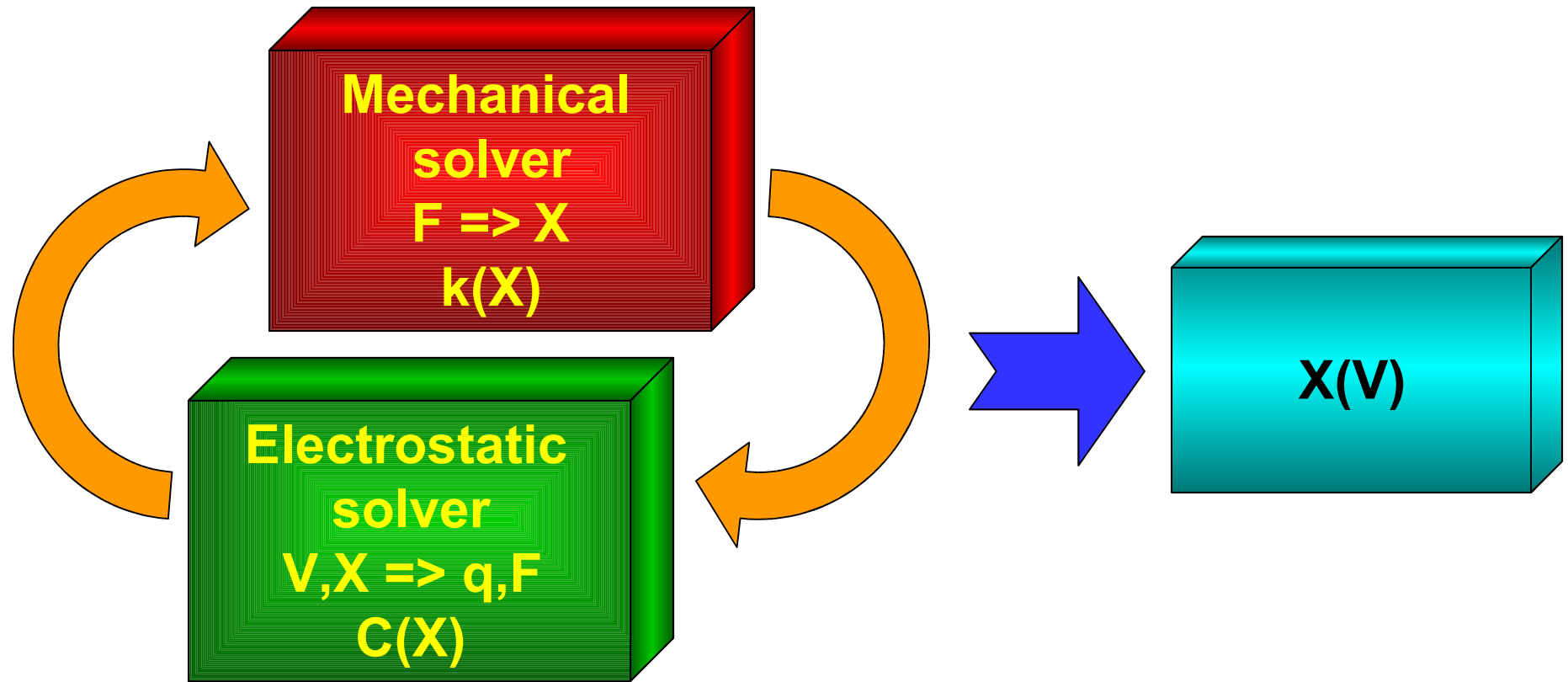
Capacitance, $C(\alpha, L, g) = L F(L \tan(\alpha)/g)/g$

Torque, $T = V^2 / 2 \frac{dC}{d\alpha} \sim (L/g)^2 \frac{dF}{d\alpha}$

snap-down angle, α_{sd} scales as g/L

- As long as $g \ll L$, works for arbitrary electrode shape.
- Analytical solution can be obtained for more than 1 DOF.
- Does not work if edge effects are important, e.g. $g \sim L$.

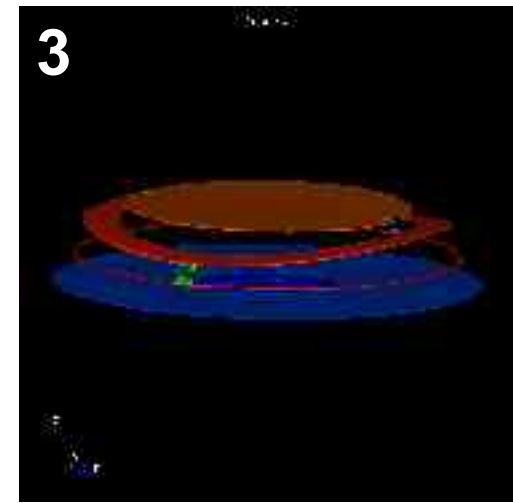
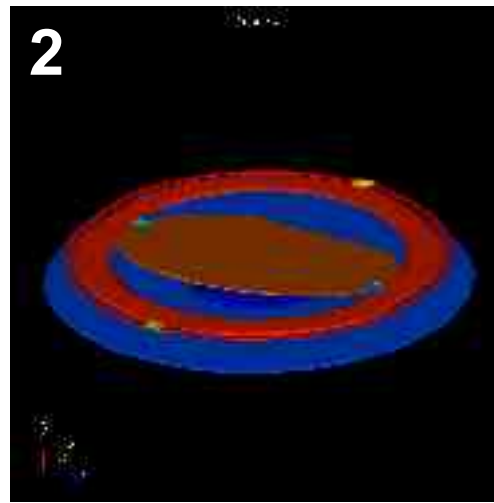
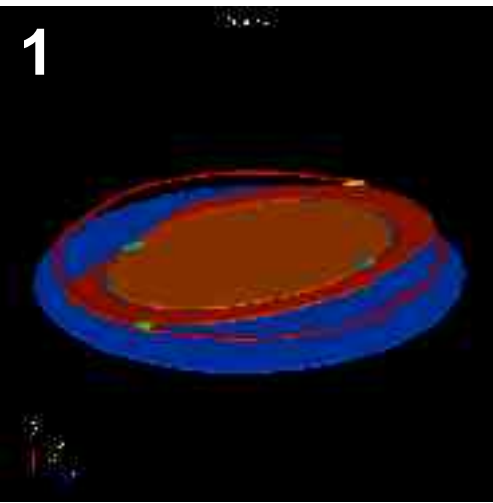
Numerical Techniques: Iterative Solver



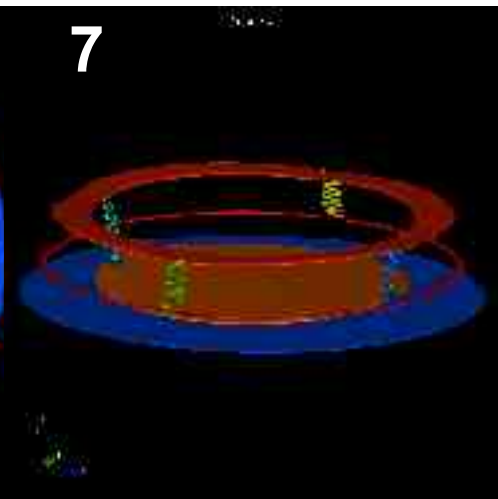
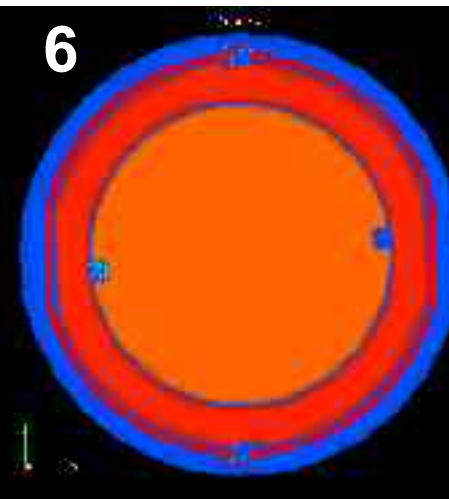
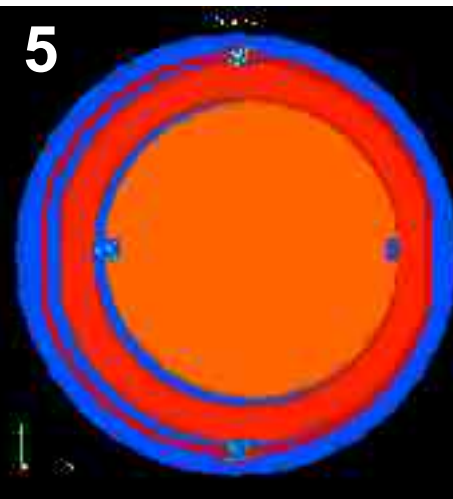
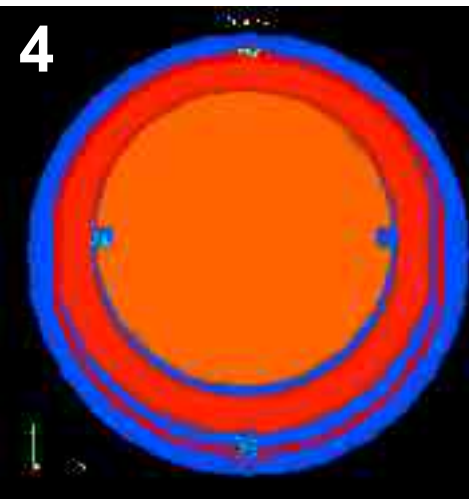
Exact calculations of mechanically deforming conductors

~ 10 cycles per device position, very time consuming for multiple trajectories.

Do we really need coupled analysis?

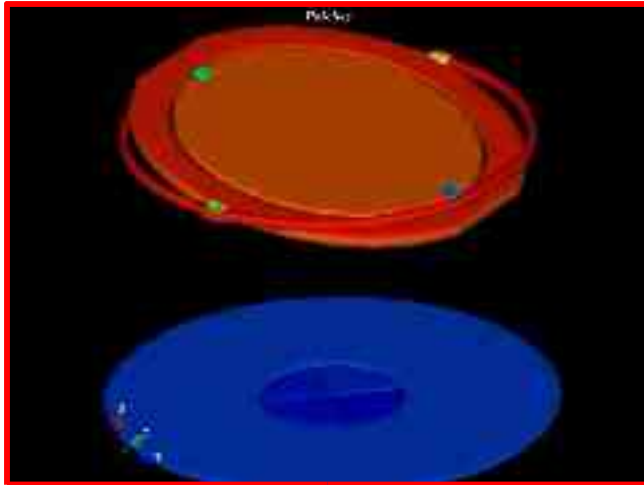


- This mirror moves as a collection of rigid bodies attached by springs
- Springs do not contribute to electrostatic force



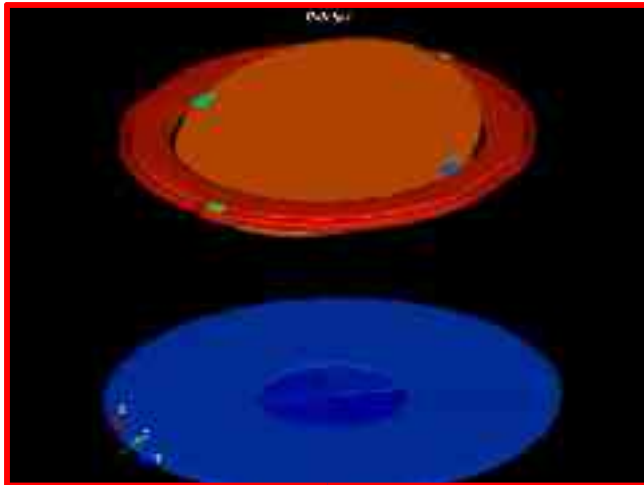
Mirror Moves As Solid Body

Tilts are the important DOF



Θ_x

Θ_y



Mechanics: $\vec{F} = \hat{K}(\vec{x}) \cdot \vec{x}$

Electrostatics: $E = \frac{1}{2} V_i V_j C_{ij}(\vec{x})$

Force or torque: $\vec{F} = \nabla E(\vec{x})$

Equilibrium: $\hat{K}(\vec{x}) \cdot \vec{x} = \frac{V_i V_j}{2} \nabla C_{ij}(\vec{x})$

E.g. 1D tilt case: $\tau = \frac{1}{2} V_i V_j \frac{dC_{ij}}{d\theta}$

No need to iterate:

- calculate τ once (Mechanical solver)
- calculate $C(\theta)$ for all θ once (Electrostatic solver)
- calculate $V(\theta)$ using the above equation

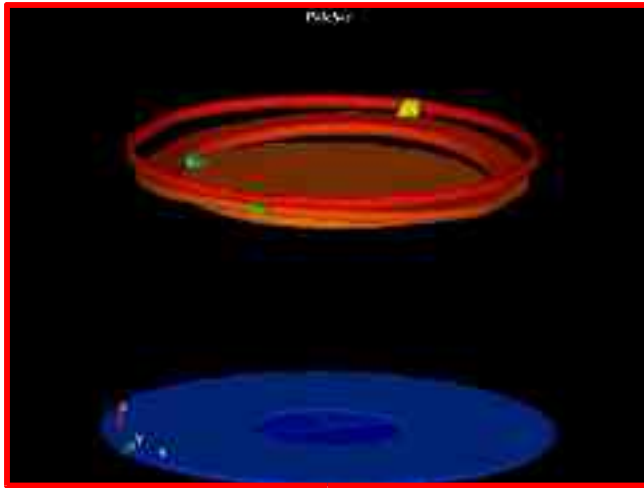
Works for two tilt angles and voltages as well.

More DOF - NO PROBLEM

Treat Z sag as perturbation

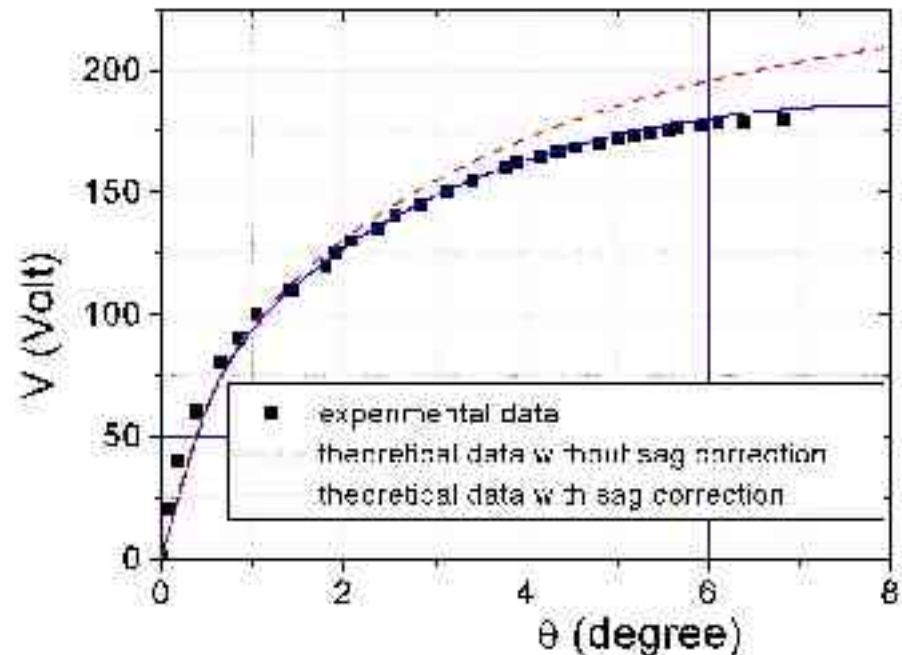
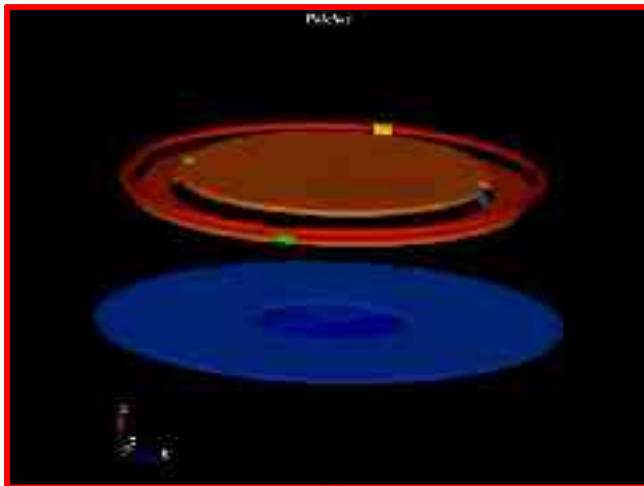
$$\hat{K}(\vec{x}) \cdot \vec{x} = \frac{V_i V_j}{2} \nabla C_{ij}(\vec{x})$$

1. Calculate $V_0(\theta, z=0)$ as before
2. Calculate $z_1(\theta, V_0)$ solving the same equation
3. Calculate new voltage $V_1(\theta, z_1(\theta))$
4. Iterate 2, 3

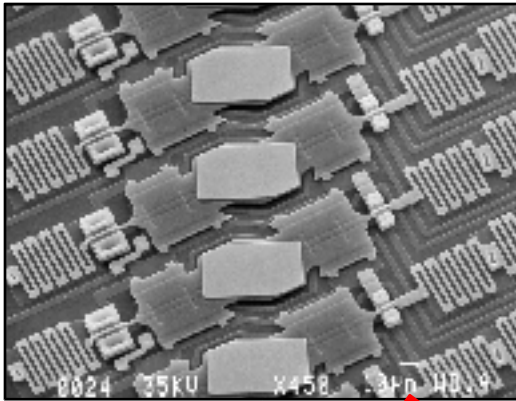


$z_m + z_g$

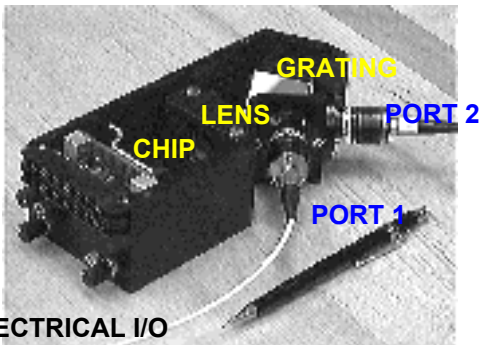
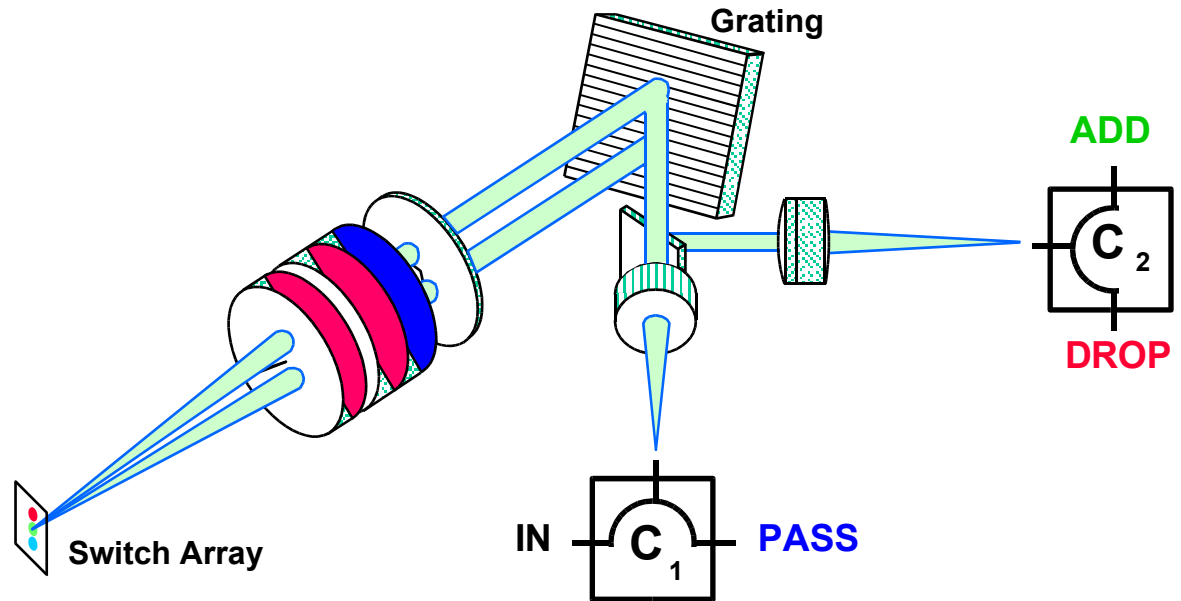
$z_m - z_g$



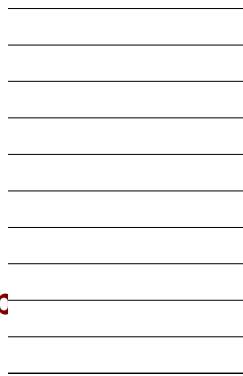
Early MEMS Wavelength-Selective Add/Drop



Tilt-Mirror Switches



ELECTRICAL I/O

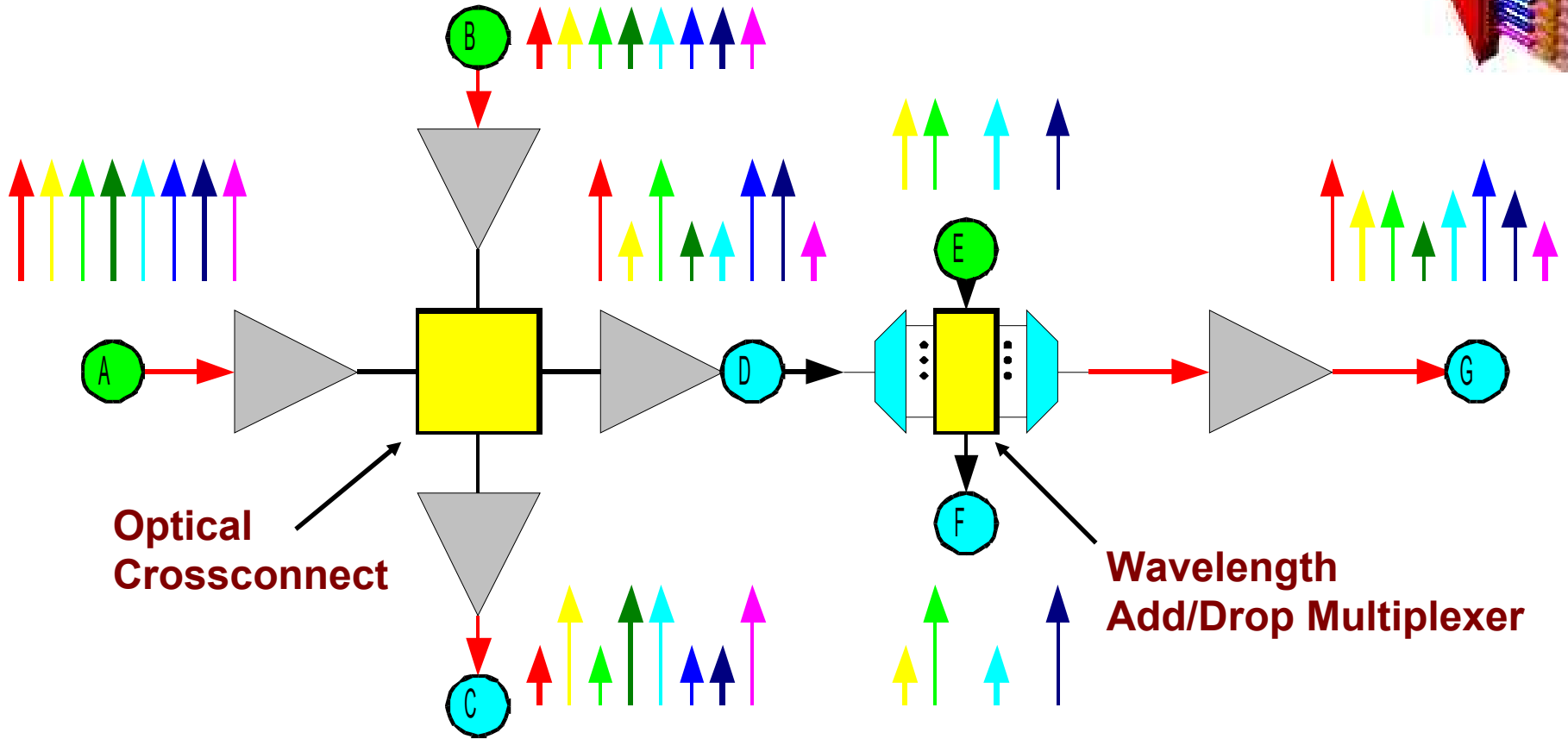
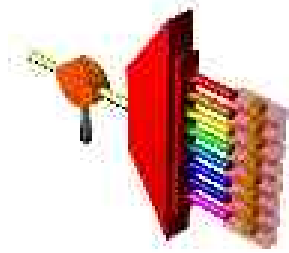


Column C



- 5 dB insertion loss (pass), 8 dB (drop)
- > 30 dB switching contrast
- 20 μ s switching of 16 λ 's @ 200 GHz

Equalization in Lightwave Networks



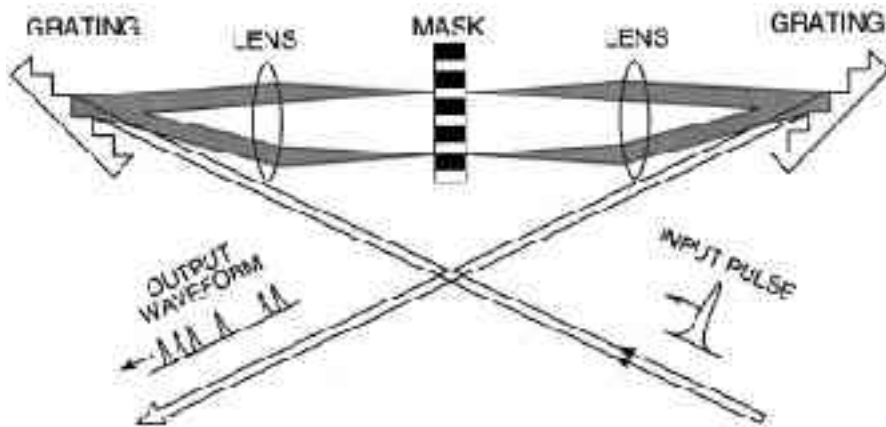
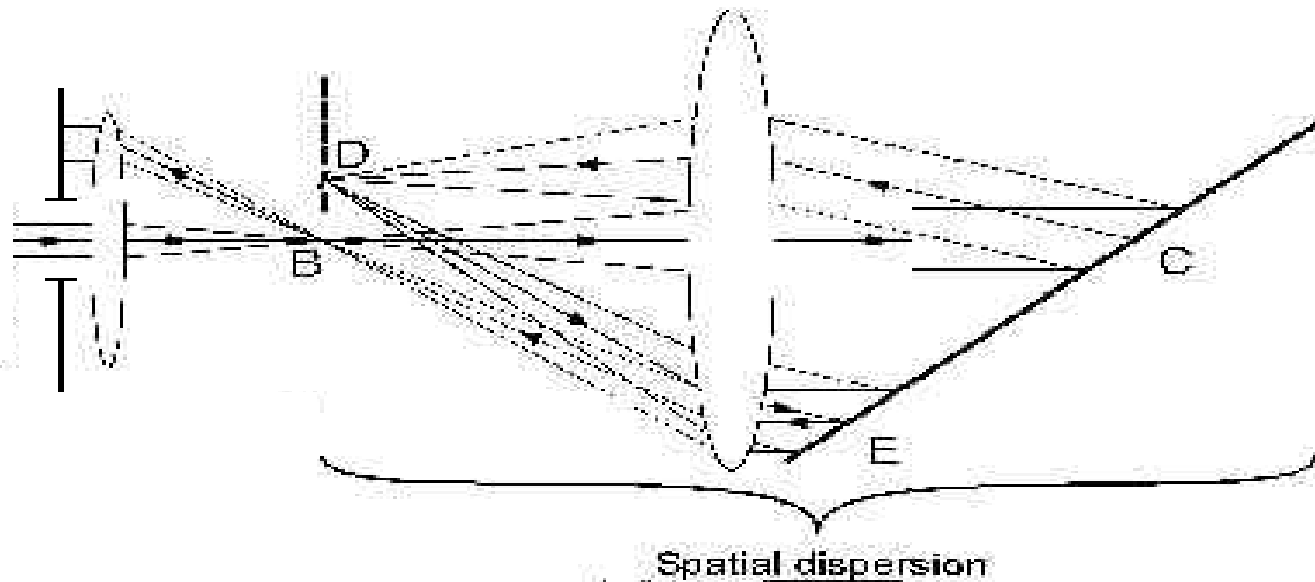
Optical Crossconnect

Wavelength Add/Drop Multiplexer

- Different line levels from **A** and **B** into crossconnect
- Different input and add levels from **D** and **E** into WADM
- Different channel losses through crossconnect and WADM
- Different channel gain and loss through optical amplifiers and fiber

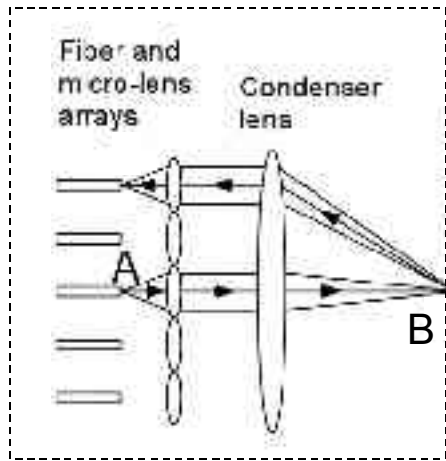
WSS for DWDM and Pulse Shaping

Phase-only SLM imparts amplitude change via spatial filtering

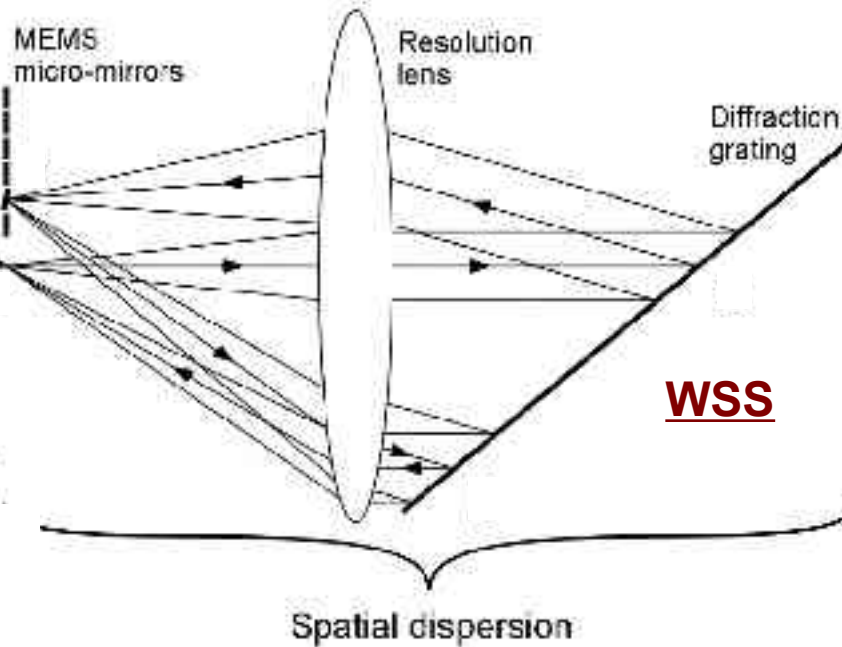
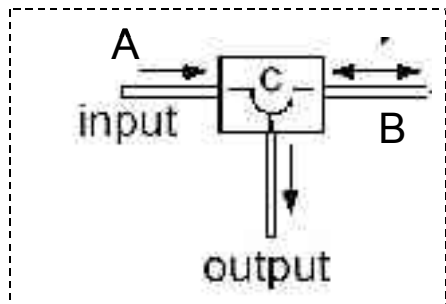


Basic layout for Fourier transform femtosecond pulse shaping.

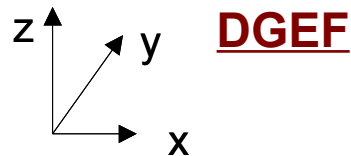
Wavelength-Selective Switch and Dynamic Gain Equalizing Filter



Space to displacement conversion or single output:



- >100 λ 's @ 100 GHz
- low loss, high contrast
- wide, flat passband (high fill factor mirrors)
- variable attenuation (analog tilt control)

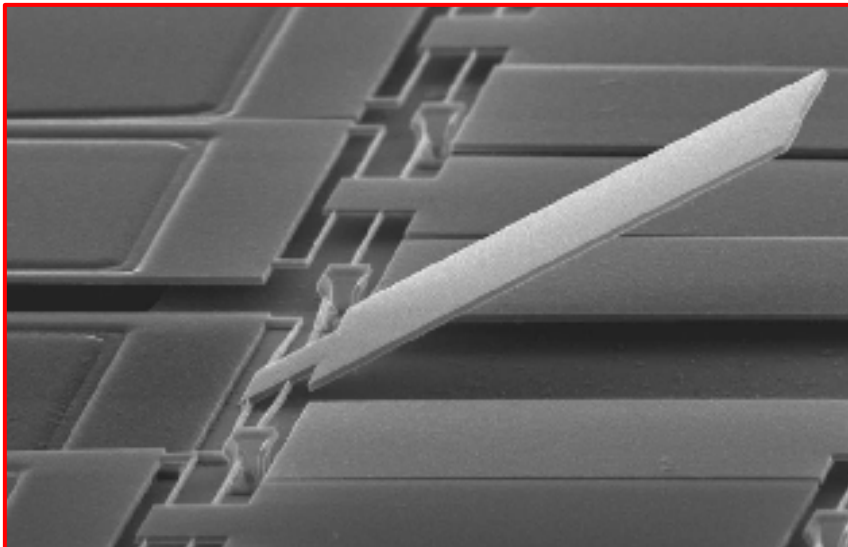
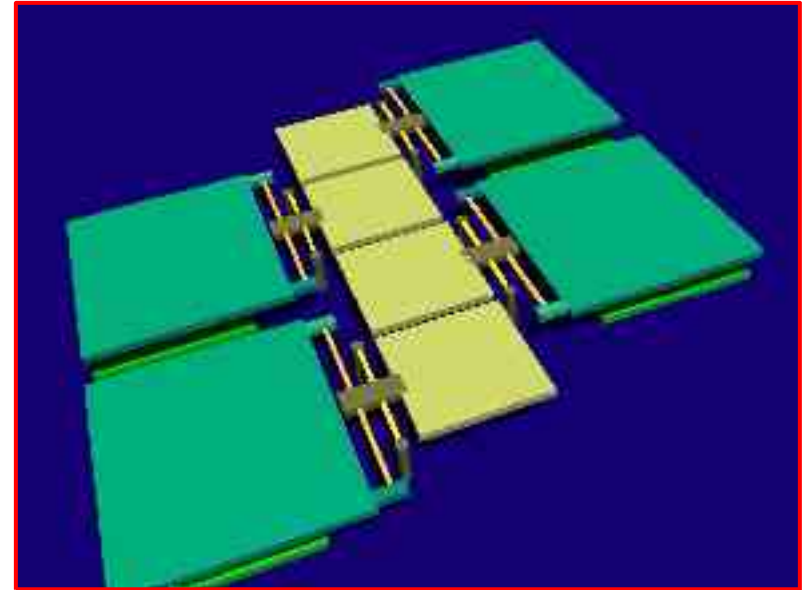


Tilt along or perpendicular to the dispersion direction.
 Similar to Femtosecond Pulse Shaping setup with MEMS mirror array as the SLM.

Double Hinge Tilting Mirror

- 10 degrees of continuous tilt
- 30 x 50 um mirrors
- moderate $V < 100V$
- high speed, $f > 10kHz$

- high fill factor (close-packed)
- no electromechanical crosstalk
- surface-micromachined



**Angle amplification enables
a more efficient actuation
regime**

**Micromechanical
transmission mechanism**

Angle Amplification

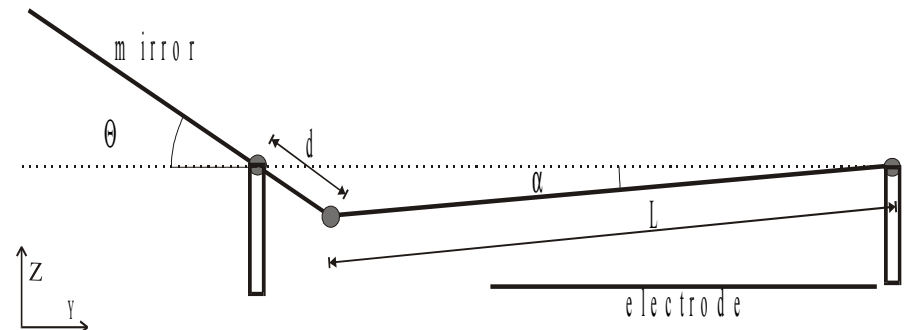
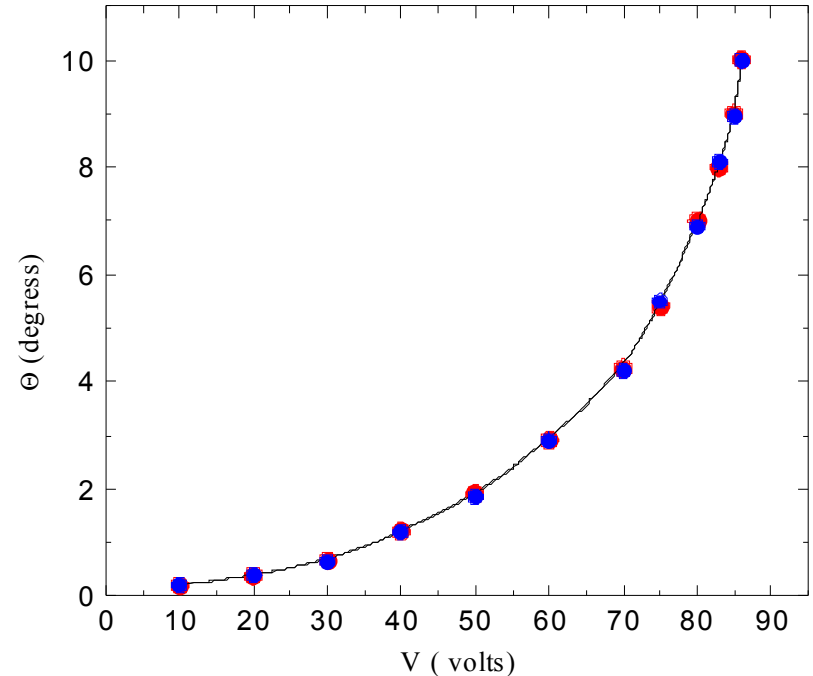
$$\sin(\theta) = \frac{L}{d} \sin(\alpha)$$

For an actuator consisting of plates, maximum output work is typically:

$$W_{\max} \propto \frac{A}{g} V^2$$

The *transmission mechanism* increases work produced by the actuator:

- larger area can be used
 - actuator gap can be decreased,
- while maintaining the required range of motion



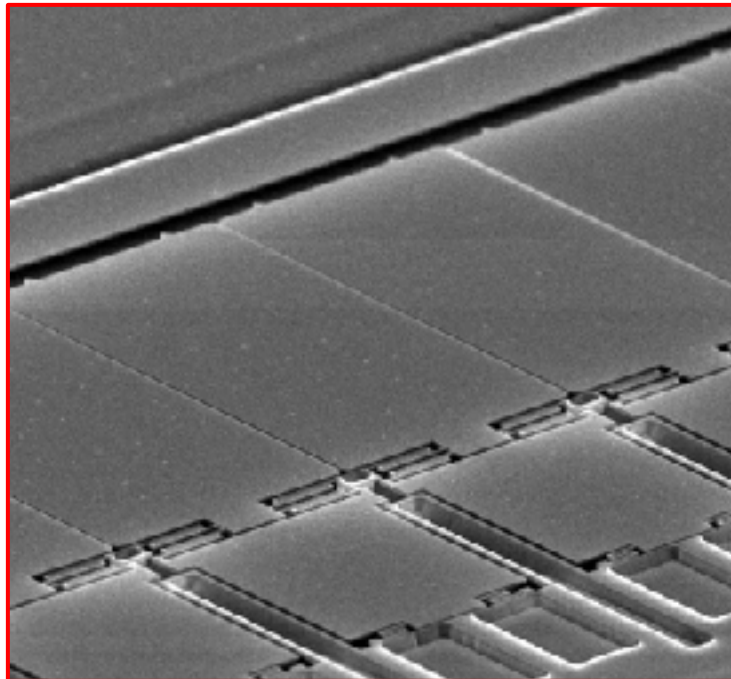
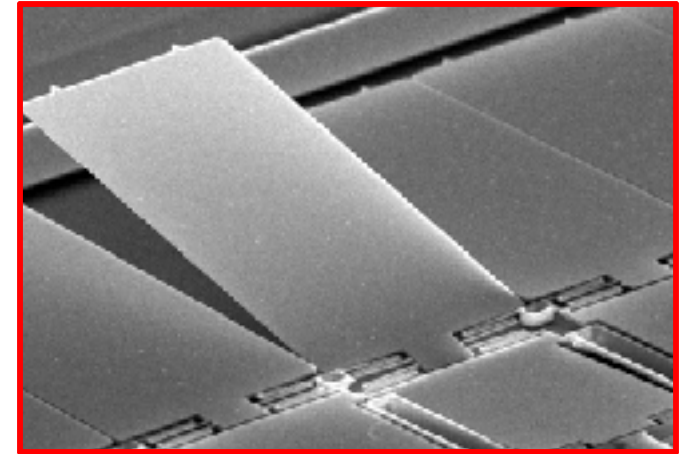
Transmission Mechanism Efficiency

$$W_{\text{electrostatic}} = E_{\text{mech}}^{\text{required}} + E_{\text{mech}}^{\text{other}} = E_{\text{mech}}^{\text{torsional}} + E_{\text{mech}}^Z$$

$$E_{\text{mech}}^{\text{torsional}} = \frac{1}{2} \tau \theta$$

$$E_{\text{mech}}^Z = \frac{1}{2} K_Z z^2$$

$$\eta = \frac{E_{\text{mech}}^{\text{required}}}{W_{\text{electrostatic}}} \rightarrow \tau \quad \left/ \quad d^2 \ll K_Z \right.$$



To maximize efficiency, need to increase stiffness to unwanted deformations:
nonlinear -

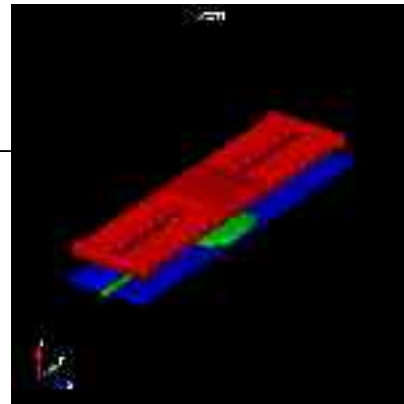
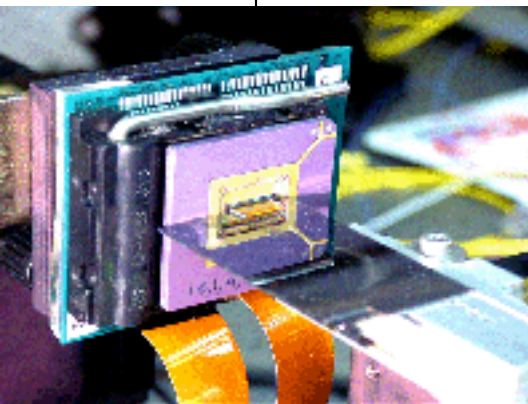
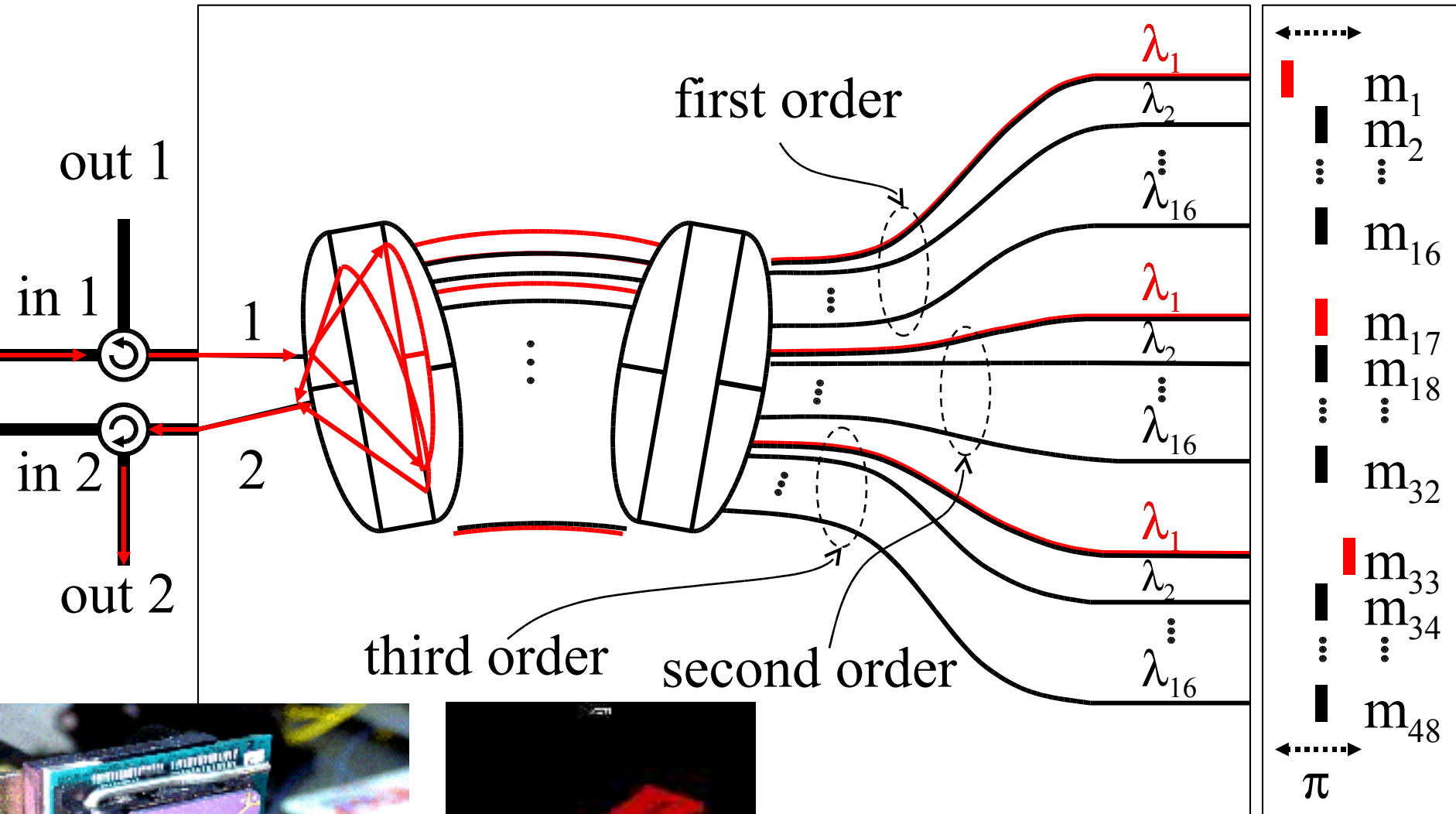
- mechanical contact - friction
- straight torsion rod - stress sensitivity

linear -

- high aspect ratio spring
- submicron lithography

WSS with MEMS and Waveguides

MEMS chip



D. Fuchs et. al. ECOC2002 PostDeadline



Complex Optical MEMS Components – What is next?

Demonstrated applications:

- Optical switches
- Displays (TI DMD)
- Adaptive optics
- Femtosecond pulse shapers
- Programmable correlation spectrometers

MEMS devices:

- mirrors arrays
- tilt or piston
- 1D or 2D
- 10um to 1mm
- 50% to 98% spatial fill factor

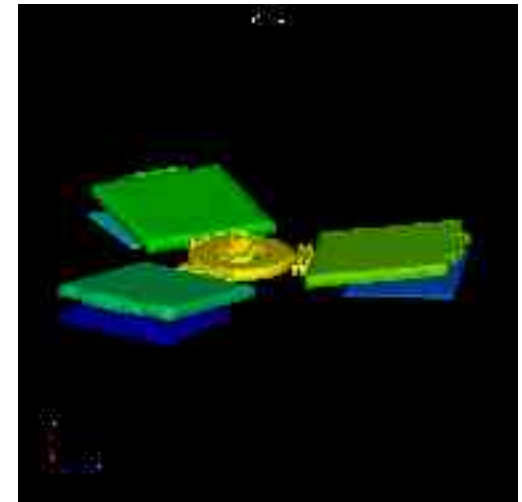
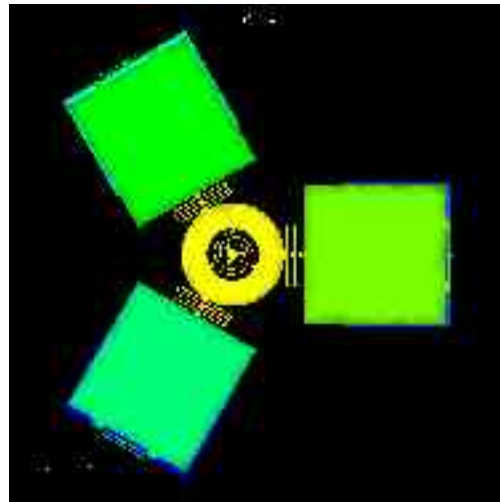
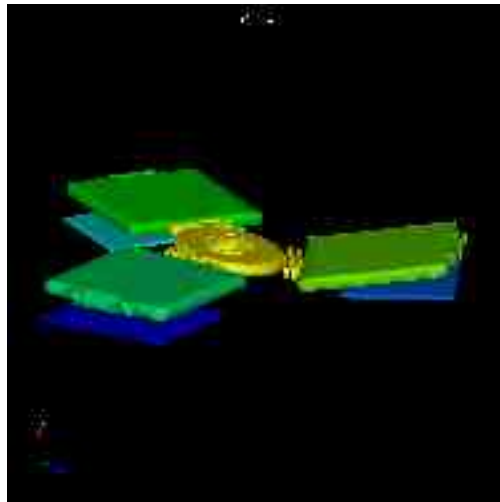
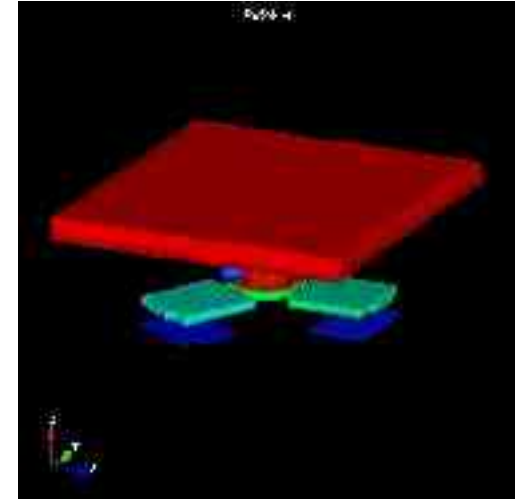
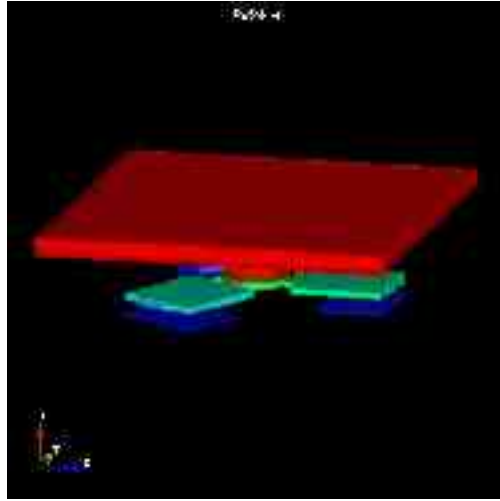
Superset: *Programmable Reflective MEMS Spatial Light Modulator (SLM):*

- Combines Tilt and Piston motion
- High reflectivity
- High fill factor
- Small, fast elements
- 2D array scalable to 1M elements
- Programmable wavefront shape – Digitally controlled thin phase holograms

“Dial in” a compound optical element:

- variable curvature
- fast tracking
- optical information processing
- optical vortices
- holographic optical tweezers
-

Concept Tilt-Piston Mirror with Angle Amplification



Some Current Research Directions for Optical MEMS at Lucent

Micro- and Nano- fabrication:

Processing for nanoscale mechanical features: combs, spring beams, vias, etc.

Electronics integration -

- Through Wafer Interconnect
- Ultra-dense chip- and wafer- scale bonding (millions of nano-bumps)
- New MEMS materials for monolithic integration with ICs

Low stress reflective micromirror coatings

Large clear aperture – processing large Si chips

...

Microsystems Design:

Lighter, stiffer, higher reflectivity mirror structures

Actuators-

- Higher power (fast, large amplitude, low voltage)
- Combining piston, tip and tilt

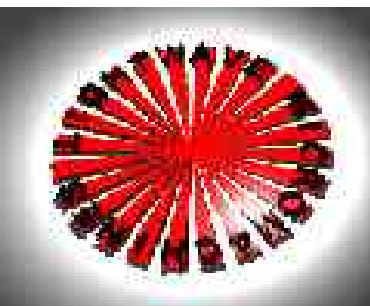
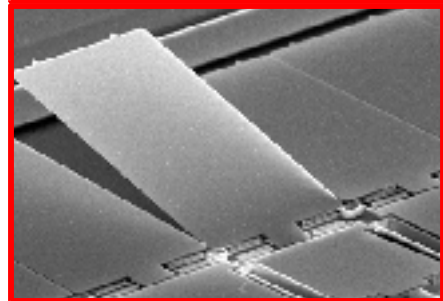
High fill factor 2D mirror arrays

Extreme high packing density, small pixel size, megapixels/chip

...

Summary

- Microscopic optomechanical components retain excellent optical properties of their macro counterparts, but are *smaller, faster, cheaper*.
- Integration of multiple mechanisms enables *new system functions*: optical crossconnects, WDM add-drops, gain equalizers.
- Scale-specific design approaches result in the best performance: *compliant mechanisms, electrostatic actuation, stress engineering*.
- Large MEMS SLMs can now be built and are likely to enable *new and interesting optical systems*.



**Optical MEMS is
an enabling technology
for optical systems**